

681

## SUPPLEMENTARY MATERIALS

## 682 Theoretical model for the optoacoustic continuum system

683 Backward Brillouin anti-Stokes scattering in a typical optical waveguide is an optoacoustic interaction between an  
 684 optical pump wave, a scattered optical anti-Stokes wave, and an acoustic wave. The dynamics of this optoacoustic  
 685 interaction can be given by

$$\begin{aligned} \frac{\partial a_p}{\partial t} + v_{\text{opt}} \frac{\partial a_p}{\partial z} &= -\frac{\gamma_{\text{opt}}}{2} a_p - i g_0 a_{\text{aS}}^\dagger b_{\text{ac}} + \sqrt{\gamma_{\text{opt}}} \xi_p, \\ \frac{\partial a_{\text{aS}}}{\partial t} - v_{\text{opt}} \frac{\partial a_{\text{aS}}}{\partial z} &= -\frac{\gamma_{\text{opt}}}{2} a_{\text{aS}} - i g_0 a_p b_{\text{ac}} + \sqrt{\gamma_{\text{opt}}} \xi_{\text{aS}}, \\ \frac{\partial b_{\text{ac}}}{\partial t} - v_{\text{ac}} \frac{\partial b_{\text{ac}}}{\partial z} &= -\frac{\Gamma_m}{2} b_{\text{ac}} - i g_0 a_p^\dagger a_{\text{aS}} + \sqrt{\Gamma_m} \xi_{\text{ac}}, \end{aligned} \quad (5)$$

686 where  $a_p(z, t)$ ,  $a_{\text{aS}}(z, t)$ , and  $b_{\text{ac}}(z, t)$  correspond to the envelope bosonic operators of the pump, anti-Stokes, and  
 687 linewidth ( $\Gamma_m$ ) and group velocity ( $v_{\text{ac}}$ ) denote the linewidth and group velocity for the optical (acoustic) wave,  
 688 respectively.  $g_0$  is the vacuum coupling strength.  $\xi_p$ ,  $\xi_{\text{aS}}$ , and  $\xi_{\text{ac}}$  are quantum Langevin noises corresponding to these  
 689 three waves, which obey the following statistical properties

$$\begin{aligned} \langle \xi_p(t, z) \rangle &= \langle \xi_{\text{aS}}(t, z) \rangle = \langle \xi_{\text{ac}}(t, z) \rangle = 0, \\ \langle \xi_p^\dagger(t_1, z_1) \xi_p(t_2, z_2) \rangle &= \langle \xi_{\text{aS}}^\dagger(t_1, z_1) \xi_{\text{aS}}(t_2, z_2) \rangle = 0, \\ \langle \xi_{\text{ac}}^\dagger(t_1, z_1) \xi_{\text{ac}}(t_2, z_2) \rangle &= n_{\text{th}} \delta(t_1 - t_2) \delta(z_1 - z_2), \end{aligned} \quad (6)$$

690 where  $n_{\text{th}} = 1/(e^{\hbar\Omega_{\text{ac}}/k_B T} - 1)$  denotes the thermal phonon occupation of the acoustic wave at temperature  $T$ .  
 691 In the undepleted pump regime where the reduction of pump power can be ignored, the three-wave interaction  
 692 can be reduced a linearized beamsplitter interaction between anti-Stokes photons and acoustic phonons with an  
 693 effective pump-enhanced coupling strength  $g_{\text{om}} = g_0 \sqrt{\langle a_p^\dagger a_p \rangle}$ . Therefore, the dynamics of the linearized optoacoustic  
 694 interaction can be expressed as follows

$$\begin{aligned} \frac{\partial a_{\text{aS}}}{\partial t} - v_{\text{opt}} \frac{\partial a_{\text{aS}}}{\partial z} &= -\frac{\gamma_{\text{opt}}}{2} a_{\text{aS}} - i g_{\text{om}} b_{\text{ac}} + \sqrt{\gamma_{\text{opt}}} \xi_{\text{aS}}, \\ \frac{\partial b_{\text{ac}}}{\partial t} - v_{\text{ac}} \frac{\partial b_{\text{ac}}}{\partial z} &= -\frac{\Gamma_m}{2} b_{\text{ac}} - i g_{\text{om}} a_{\text{aS}} + \sqrt{\Gamma_m} \xi_{\text{ac}}. \end{aligned} \quad (7)$$

695 Without the cavity structure, the optical anti-Stokes and acoustic waves contains continuously accessible groups of  
 696 optical photons and acoustic phonons, respectively, i.e., envelope bosonic operators  $a_{\text{aS}}(z, t)$  and  $b_{\text{ac}}(z, t)$  at position  
 697  $z$  along the 1D waveguide can be constructed as

$$a_{\text{aS}}(z, t) = \frac{1}{2\pi} \int dk \, a(k, t) e^{-ikz}, \quad b_{\text{ac}}(z, t) = \frac{1}{2\pi} \int dk \, b(k, t) e^{-ikz}, \quad (8)$$

698 where  $a(k, t)$  and  $b(k, t)$  are annihilation operators for the  $k$ -th Stoke photon mode and acoustic phonon mode with  
 699 wave number  $k$ . Moving into momentum space, Eq. (7) can be rewritten as

$$\begin{aligned} \frac{da(k, t)}{dt} &= \left( -\frac{\gamma_{\text{opt}}}{2} + i\Delta_{\text{as}} \right) a - i g_{\text{om}} b + \sqrt{\gamma_{\text{opt}}} \xi_a, \\ \frac{db(k, t)}{dt} &= \left( -\frac{\Gamma_m}{2} + i\Delta_{\text{ac}} \right) b - i g_{\text{om}} a + \sqrt{\Gamma_m} \xi_b, \end{aligned} \quad (9)$$

700 where  $k$  is the wave number in the momentum space. We can see that Eq. (9) describes a beamsplitter interaction  
 701 between the  $k$ -th photon and phonon modes with interaction Hamiltonian  $H_{\text{int}} = \hbar g_{\text{om}}(a^\dagger(k, t)b(k, t) + b^\dagger(k, t)a(k, t))$ .  
 702 Moving into the frequency domain via a Fourier transformation, Eq. (9) can be re-expressed as

$$\begin{aligned} -i\omega \tilde{a}(k, \omega) &= \left( -\frac{\gamma_{\text{opt}}}{2} + i\Delta_{\text{as}} \right) \tilde{a}(k, \omega) - i g_{\text{om}} \tilde{b}(k, \omega) + \sqrt{\gamma_{\text{opt}}} \tilde{\xi}_a(k, \omega), \\ -i\omega \tilde{b}(k, \omega) &= \left( -\frac{\Gamma_m}{2} + i\Delta_{\text{ac}} \right) \tilde{b}(k, \omega) - i g_{\text{om}} \tilde{a}(k, \omega) + \sqrt{\Gamma_m} \tilde{\xi}_b(k, \omega), \end{aligned} \quad (10)$$

703 where  $\tilde{a}$ ,  $\tilde{b}$ ,  $\tilde{\xi}_a$ , and  $\tilde{\xi}_b$  correspond to the Fourier transform of  $a$ ,  $b$ ,  $\xi_a$ , and  $\xi_b$ . The solutions of above equations can  
704 be given by

$$\begin{aligned}\tilde{a}(k, \omega) &= \frac{\left(\frac{\Gamma_m}{2} - i(\omega + \Delta_{ac})\right) \sqrt{\gamma_{\text{opt}}} \tilde{\xi}_a(\omega) - ig_{\text{om}} \sqrt{\Gamma_m} \tilde{\xi}_b(\omega)}{g_{\text{om}}^2 + \left(\frac{\gamma_{\text{opt}}}{2} - i(\omega + \Delta_{\text{as}})\right) \left(\frac{\Gamma_m}{2} - i(\omega + \Delta_{ac})\right)}, \\ \tilde{b}(k, \omega) &= \frac{-ig_{\text{om}} \sqrt{\gamma_{\text{opt}}} \tilde{\xi}_a(\omega) + \left(\frac{\gamma_{\text{opt}}}{2} - i(\omega + \Delta_{\text{as}})\right) \sqrt{\Gamma_m} \tilde{\xi}_b(\omega)}{g_{\text{om}}^2 + \left(\frac{\gamma_{\text{opt}}}{2} - i(\omega + \Delta_{\text{as}})\right) \left(\frac{\Gamma_m}{2} - i(\omega + \Delta_{ac})\right)}.\end{aligned}\quad (11)$$

705 We define the quadrature operators and the corresponding Fourier transform of anti-Stokes and acoustic modes as  
706 follows

$$\begin{aligned}X_a(k, t) &= \frac{a^\dagger(k, t) + a(k, t)}{\sqrt{2}}, \quad Y_a(k, t) = \frac{a(k, t) - a^\dagger(k, t)}{\sqrt{2}i}, \\ \tilde{X}_b(k, t) &= \frac{\tilde{b}^\dagger(k, t) + \tilde{b}(k, t)}{\sqrt{2}}, \quad \tilde{Y}_b(k, t) = \frac{\tilde{b}^\dagger(k, t) - \tilde{b}(k, t)}{\sqrt{2}i}.\end{aligned}\quad (12)$$

707 Thus we have

$$\langle \tilde{X}_a^\dagger(\omega_1) \tilde{X}_a(\omega_2) \rangle = 2\pi S_{XX}^{\text{as}}(\omega_1) \delta(\omega_1 - \omega_2), \quad (13)$$

708 where  $S_{XX}^{\text{as}}(k, \omega)$  denotes the displacement spectrum for the  $k$ -th anti-Stokes mode. Based on Eq. (6), the Langevin  
709 noises of  $\tilde{\xi}_a$  and  $\tilde{\xi}_b$  obey correlation relationships as follows

$$\begin{aligned}\langle \tilde{\xi}_a^\dagger(k, \omega_1) \tilde{\xi}_a(k, \omega_2) \rangle &= 0, \\ \langle \tilde{\xi}_a(k, \omega_1) \tilde{\xi}_a^\dagger(k, \omega_2) \rangle &= 2\pi \delta(\omega_1 - \omega_2), \\ \langle \tilde{\xi}_b^\dagger(k, \omega_1) \tilde{\xi}_b(k, \omega_2) \rangle &= 2\pi n_{\text{th}} \delta(\omega_1 - \omega_2), \\ \langle \tilde{\xi}_b(k, \omega_1) \tilde{\xi}_b^\dagger(k, \omega_2) \rangle &= 2\pi (n_{\text{th}} + 1) \delta(\omega_1 - \omega_2).\end{aligned}\quad (14)$$

710 According to noise correlations Eq. (14) and solution of anti-Stokes mode Eq. (11), we have

$$\begin{aligned}\langle \tilde{a}^\dagger(\omega_1) \tilde{a}(\omega_2) \rangle &= \frac{2\pi g_{\text{om}}^2 \Gamma_m n_{\text{th}} \delta(\omega_1 - \omega_2)}{\left|g_{\text{om}}^2 + \left(\frac{\gamma_{\text{opt}}}{2} + i(\omega_1 + \Delta_{\text{as}})\right) \left(\frac{\Gamma_m}{2} + i(\omega_1 + \Delta_{\text{ac}})\right)\right|^2}, \\ \langle \tilde{a}(\omega_1) \tilde{a}^\dagger(\omega_2) \rangle &= 2\pi \frac{\gamma_{\text{opt}} \left(\frac{\Gamma_m^2}{4} + (\omega_1 + \Delta_{\text{ac}})^2\right) + g_{\text{om}}^2 \Gamma_m (n_{\text{th}} + 1)}{\left|g_{\text{om}}^2 + \left(\frac{\gamma_{\text{opt}}}{2} + i(\omega_1 + \Delta_{\text{as}})\right) \left(\frac{\Gamma_m}{2} + i(\omega_1 + \Delta_{\text{ac}})\right)\right|^2} \delta(\omega_1 - \omega_2), \\ \langle \tilde{a}^\dagger(\omega_1) \tilde{a}^\dagger(\omega_2) \rangle &= 0, \\ \langle \tilde{a}(\omega_1) \tilde{a}(\omega_2) \rangle &= 0.\end{aligned}\quad (15)$$

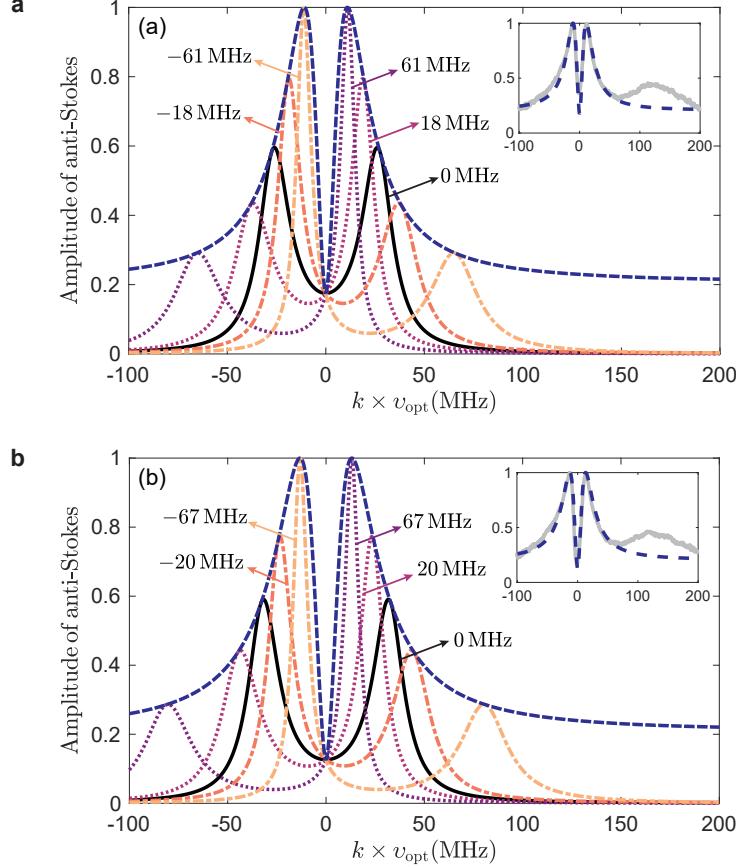
711 Thus we have

$$\begin{aligned}&\langle \tilde{X}_a^\dagger(\omega_1) \tilde{X}_a(\omega_2) \rangle \\ &= \frac{\langle \tilde{a}^\dagger(\omega_1) \tilde{a}(\omega_2) \rangle + \langle \tilde{a}(\omega_1) \tilde{a}^\dagger(\omega_2) \rangle + \langle \tilde{a}^\dagger(\omega_1) \tilde{a}^\dagger(\omega_2) \rangle + \langle \tilde{a}(\omega_1) \tilde{a}(\omega_2) \rangle}{2} \\ &= 2\pi \frac{\frac{\gamma_{\text{opt}}}{2} \left(\frac{\Gamma_m}{2} + (\omega_1 + \Delta_{\text{ac}})^2\right) + \frac{\Gamma_m}{2} g_{\text{om}}^2 (2n_{\text{th}} + 1)}{\left(g_{\text{om}}^2 + \frac{\gamma_{\text{opt}} \Gamma_m}{4} - (\omega_1 + \Delta_{\text{as}})(\omega_1 + \Delta_{\text{ac}})\right)^2 + \frac{1}{4} (\gamma_{\text{opt}}(\omega_1 + \Delta_{\text{ac}}) + \Gamma_m(\omega_1 + \Delta_{\text{as}}))^2} \delta(\omega_1 - \omega_2),\end{aligned}\quad (16)$$

712 By comparing Eq. (13) and Eq. (16), the displacement spectrum of the  $k$ -th anti-Stokes mode can be given by

$$S_{XX}^{\text{as}}(k, \omega) = \frac{\frac{\gamma_{\text{opt}}}{2} \left(\frac{\Gamma_m}{2} + (\omega + \Delta_{\text{ac}})^2\right) + \frac{\Gamma_m}{2} g_{\text{om}}^2 (2n_{\text{th}} + 1)}{\left(g_{\text{om}}^2 + \frac{\gamma_{\text{opt}} \Gamma_m}{4} - (\omega + \Delta_{\text{as}})(\omega + \Delta_{\text{ac}})\right)^2 + \frac{1}{4} (\gamma_{\text{opt}}(\omega + \Delta_{\text{ac}}) + \Gamma_m(\omega + \Delta_{\text{as}}))^2}. \quad (17)$$

713 We show simulation results of spectra for anti-Stokes modes under the strong coupling regime in Fig. 5 (a) and (b).  
714 The dotted and dash-dot curves denote spectra of optical anti-Stokes modes for positive and negative wave number  $k$ ,  
715 respectively. The black solid curve corresponds to the phase-matching case, i.e.,  $k = 0$ . We can see that in the strong  
716 coupling regime, each anti-Stokes mode exhibits the normal-mode splitting. When the wave number  $k$  changes from



**FIG. 5. Simulation results of spectra for the anti-Stokes wave.** (a) The spectra of anti-Stokes wave with pump power of 0.83 W for various wave number  $k$ , where dotted (dash-dot) lines denote the spectrum of  $k$ -th anti-Stokes mode with positive (negative) wave number  $k$  and the black solid line correspond to the phase-matching case ( $k = 0$ ). The dark blue dashed line shows the envelope of spectra for anti-Stokes modes with continuous wave number  $k$ . The inset indicates that experiment results (grey solid line) agree well with theoretical results (dark blue dashed line). (b) corresponds to the spectra of anti-Stokes wave with pump power of 1.21 W.

negative (dash-dot curves) to positive values (dotted curves), there is an avoided crossing, which is demonstrated in Fig. 3 in the main text. The insets in Fig. 5 (a) and (b) present the simulation (blue dashed curves) and experiment (red solid curves) results for different pump powers, which are in agreement with each other.

Similarly, the displacement spectrum for the  $k$ -th acoustic mode can be expressed as

$$S_{XX}^{\text{ac}}(k, \omega) = \frac{\frac{\gamma_{\text{opt}}}{2} \left( \frac{\Gamma_m}{2} + (\omega + \Delta_{\text{ac}})^2 \right) + \frac{\Gamma_m}{2} g_{\text{om}}^2 (2n_{\text{th}} + 1)}{\left( g_{\text{om}}^2 + \frac{\gamma_{\text{opt}} \Gamma_m}{4} - (\omega + \Delta_{\text{as}})(\omega + \Delta_{\text{ac}}) \right)^2 + \frac{1}{4} (\gamma_{\text{opt}}(\omega + \Delta_{\text{ac}}) + \Gamma_m(\omega + \Delta_{\text{as}}))^2}. \quad (18)$$

The eigenvalues of coupled anti-Stokes and acoustic modes with wave number  $k$  can be given by

$$\omega_{\pm} = -\frac{\gamma_{\text{opt}} + \Gamma_m}{4} + i \frac{\Delta_{\text{as}} + \Delta_{\text{ac}}}{2} \pm i \sqrt{g_{\text{om}}^2 - \left( \frac{\gamma_{\text{opt}} - \Gamma_m}{4} - i \frac{\Delta_{\text{as}} - \Delta_{\text{ac}}}{2} \right)^2}. \quad (19)$$

### Sample

The sample used in the experiment is a 2.5 m highly nonlinear fiber (HNLF) placed inside a 4K Helium cryostat. The higher nonlinearity comes from the higher doping of Germanium in the core compared to single mode fiber (SMF). An HNLF has the same step-index, core-cladding structure as an SMF, allowing the sample to be spliced to standard

Table I. **Brillouin parameters for different samples.** Comparison of Brillouin parameters between room temperature standard SMF and the HNLF sample used in this study at room and cryogenic temperatures. These parameters are obtained for  $\lambda_{\text{pump}} = 1550$  nm. SMF parameters from [1].

Fiber type	Temperature (K)	Length (cm)	$\Omega_B/2\pi$ (GHz)	$\Gamma_m$ (MHz)	$G_B$ ( $\text{W}^{-1}\text{m}^{-1}$ )	$g_B$ ( $\text{W}^{-1}\text{m}$ )
SMF	293	-	10.87	20	0.14	$1.19 \cdot 10^{-11}$
HNLF	293	250	9.73	46.3	1.60	$8.1 \cdot 10^{-11}$
HNLF	4	150	9.60	9.91	6	$3.2 \cdot 10^{-10}$

726 APC connectors. The cladding and core diameters for both types of fiber is 125  $\mu\text{m}$  and 8.2  $\mu\text{m}$  [2], respectively. The  
727 loss of the sample in-coupling splice is -1.48 dB and of the out-coupling splice, -1.79 dB. In order to avoid heating  
728 because of the losses of the splices, these were placed outside of the cold plate of the cryostat, resulting in a cold  
729 section of the fiber estimated to be 1.5 m length. The parameters of the sample are given in Table I, comparing with  
730 standard SMF. The optical dissipation rate for this sample is  $\gamma_{\text{opt}} = 24 \pm 2$  MHz, where  $\gamma_{\text{opt}}$  is defined as

$$\gamma_{\text{opt}} = \frac{\alpha_{\text{linear}} c}{2\pi n}, \quad (20)$$

731 where  $c$  is the speed of light in vacuum,  $n$  the material refractive index and  $\alpha_{\text{linear}}$  the linear loss.

### 732 Thermal-noise-initiated measurement

733 The setup used to perform a thermal-noise-initiated measurement via heterodyne detection is shown in Fig. 6.  
734 The continuous emission of a narrow line laser with a wavelength  $\lambda_{\text{pump}} = 1550$  nm is separated into two paths,  
735 pump and local oscillator (LO). The light in the pump arm is first amplified by a 5 W Erbium doped fiber amplifier  
736 (EDFA) and then filtered with a 0.8 nm tunable filter to remove the amplified spontaneous emission (ASE) coming  
737 from the EDFA. The pump is guided to the sample via a circulator, which redirects the back-reflected signal coming  
738 from the fiber into the detection part of the setup. As this signal will contain both the pump backreflection and the  
739 Brillouin resonance, a narrow-line tunable filter is used to selectively detect the Stokes or anti-Stokes signal. The  
740 leftover transmitted pump is dumped after the sample. An optical isolator is placed before the dump in order to  
741 reduce the back-reflected noise by 12 dB. Regarding the LO arm of the experiment, the frequency of the light is  
742 shifted 200 MHz by an acousto-optic modulator (AOM). This allows to separate the two resonances in the detection  
743 device, which is particularly important for high pump power measurements in the cryostat. As the Stokes process  
744 enters the stimulated Brillouin-Mandelstam scattering (SBS) regime, the signal becomes so strong that it can not be  
745 fully filtered out. Frequency shifting the LO allows to measure the anti-Stokes signal without perturbations. The  
746 back-reflected signal and the LO are mixed in a 90:10 coupler and the interference directed to a high speed photodiode.  
747 A polarization controller in the LO arm is used to optimize the polarization overlap and therefore the signal. Finally,  
748 the transduced optical-into-electrical signal of the photodiode is sent and analyzed by an electrical spectrum analyzer  
749 (ESA).

750 The results for the experimental study of Brillouin-Mandelstam scattering in the sample at cryogenic temperatures  
751 are shown in Fig. 7 and Fig. 8. As explained in the previous section, not the whole HNLF is at low temperature, as  
752 sections of it are outside of the base plate in order to allow splicing for optical access. This results in three regions of  
753 the fiber: cold, room temperature and transition between the two. This is reflected in the spectra shown in Fig. 7 (a).  
754 Two main peaks are present, the cold one centered at  $\Omega_B/2\pi = 9.5997 \pm 0.0001$  GHz and the room temperature  
755 one centered at  $\Omega_B/2\pi = 9.7278 \pm 0.0004$  GHz. As the pump power is increased, the cold Stokes resonance will  
756 enter the stimulated Brillouin-Mandelstam scattering regime (SBS), increasing exponentially and narrowing from  
757  $9.91 \pm 0.07$  MHz to  $5.14 \pm 0.04$  MHz. On the contrary, the anti-Stokes resonance broadens until it splits in two,  
758 meaning the strong coupling regime has been reached (Fig. 8 (a)). Having a closer look at the cold part of the spectrum  
759 for low input power (Fig. 7 (b) and Fig. 8 (b)), two peaks of different linewidths centered around 9.5997 GHz are  
760 present. A narrow 9.91 MHz peak, corresponding to the cryogenic part of the sample, and a broader  $77.2 \pm 0.7$  MHz  
761 peak. The source of this signal is the transition regions of the fiber, particularly of temperature around 190 K (Fig. 9  
762 (a)). Around that temperature, the frequency shift is the same as at 4 K (Fig. 9 (b)), but the linewidth is higher  
763 (Fig. 9 (c)) [3].

764 The fact that these three regions of temperature are present in the sample is shown in Fig. 9 (a), where three peaks  
765 are present in the spectrum, the transition region one being the faintest because of the short length of fiber that  
766 generates it. The reason why there is a length of fiber at this specific temperature long enough to generate a distinct  
767 signal could be the following. Two parts of the fiber of approximately 1 cm each are adhered with silicone tape to the

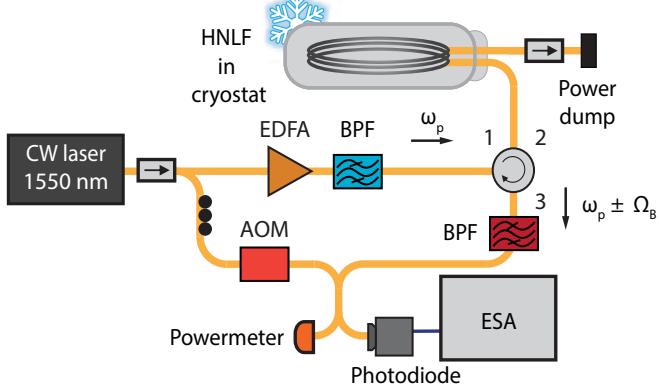


FIG. 6. **Thermal-noise-initiated experiment.** Diagram of the experimental setup used to measure thermal-noise-initiated Brillouin-Mandelstam scattering via heterodyne detection. CW: continuous wave; AOM: acousto-optical modulator; EDFA: erbium-doped fiber amplifier; BPF: band-pass filter, ESA: electrical spectrum analyzer. The three black circles represent a fiber polarization controller.

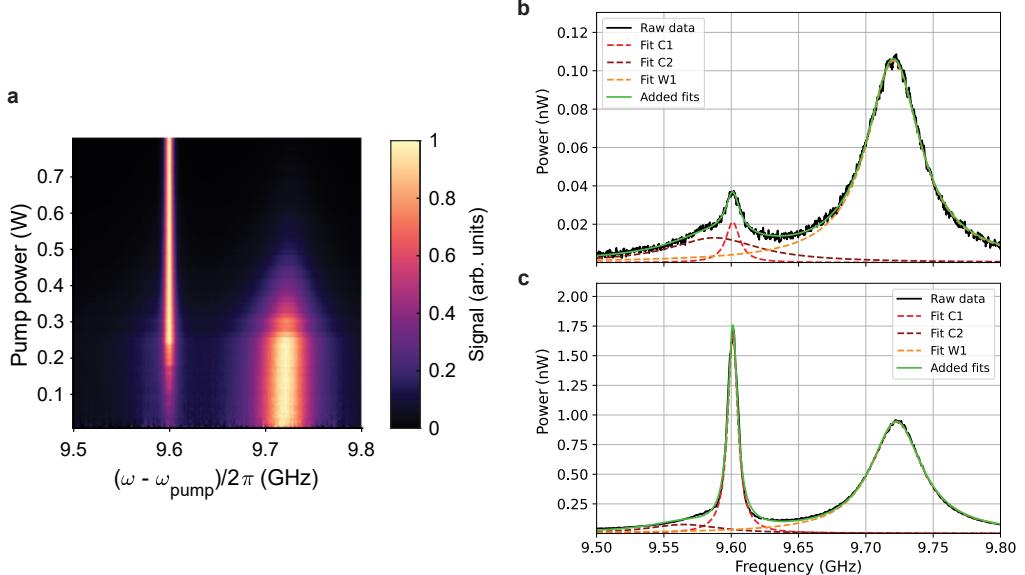


FIG. 7. **Thermal-noise-initiated measurement of Stokes resonances.** (a) Normalized Stokes Brillouin response of the sample as a function of pump power. As the pump power is increased, the resonance coming from the 4 K section (peak at 9.5997 GHz) enters the stimulated regime and increases exponentially. The response of the room temperature part (peak at 9.7278 GHz) is only visible for low powers, comparatively. (b) Spectrum of the full Stokes response of the sample at low input power. The signal centered at 9.6 GHz is composed of two peaks, a narrow 9.91 MHz one coming from the 4 K section of the fiber and a broad 77.2 MHz one coming from the transition to room temperature, at 190 K. (c) Spectrum of the full Stokes response of the sample at higher input power. The spectrum is now dominated by the narrow peak coming from the 4 K section of the fiber.

radiation shield of the cryostat, to which they are thermalized. As the rest of the fiber is suspended in vacuum, these are the only parts outside of a smooth temperature gradient. Given the short length of these sections, their response is only non-negligible at very low pump powers, in which the totality of the Brillouin response of the fiber comes from spontaneous scattering. As they are at a higher temperature than the cold part, more phonons are present there, allowing for a scattered signal to be measured. In order to calculate  $\Gamma_m$  correctly they need to be considered in the analysis. Nonetheless, for higher pump power, the response of the fiber at 9.5997 GHz mainly originates from the cold part of the fiber (Fig. 8 (c) and Fig. 7 (c)).

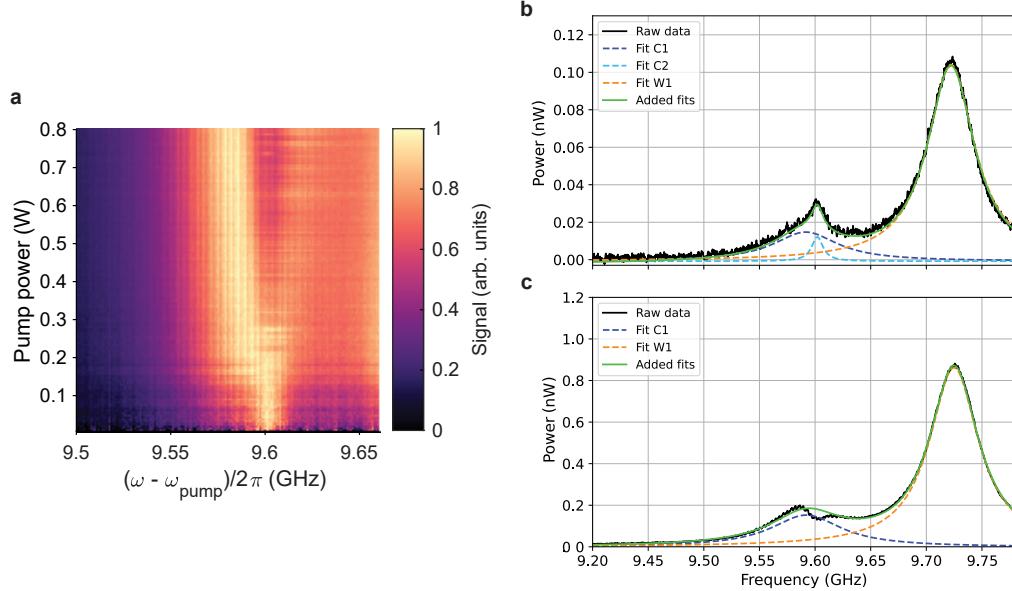


FIG. 8. **Thermal-noise-initiated measurement of anti-Stokes resonances.** (a) Normalized Anti-Stokes Brillouin response of the cryogenic sample as a function of pump power. As the pump power is increased, the resonance splits, corresponding to the transition into the strong coupling regime. (b) Spectrum of the full anti-Stokes response of the sample at low input power. Same behavior as described in 7 (b). (c) Spectrum of the full anti-Stokes response of the sample at higher input power. As the pump power increases, the signal coming from the 4 K region of the sample dominates the 9.6 GHz spectrum, showing the strong coupling splitting.

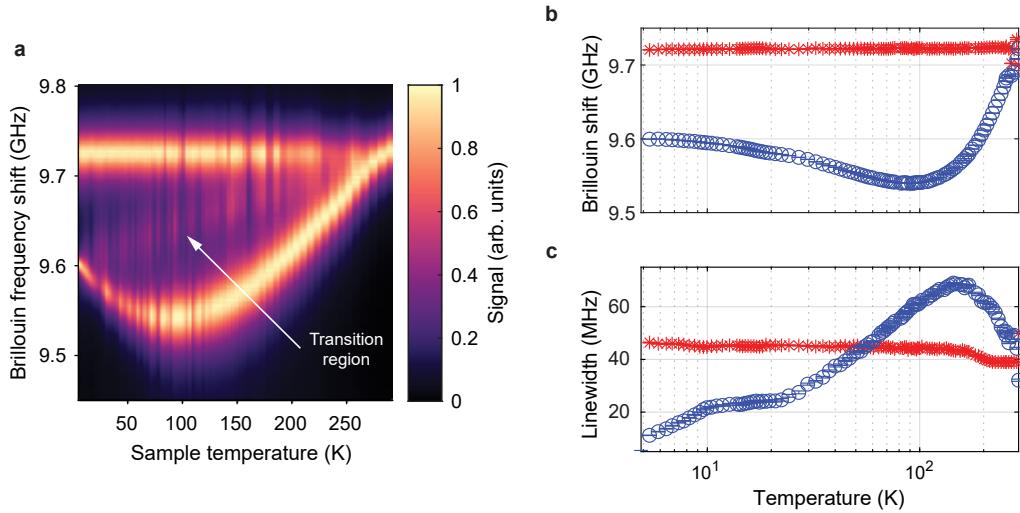


FIG. 9. **Stokes Brillouin response versus sample temperature.** (a) Stokes response of the sample as a function of sample temperature. The resonance at the top, centered at  $(\Omega_B/2\pi = 9.72$  GHz), corresponds to the room temperature part of the fiber, and it does not shift as its temperature remains constant. On the lower part of the plot, the behavior of the sections of the fiber affected by the variation of temperature is shown. The most pronounced peak corresponds to the fiber section on the base plate of the cryostat. A faint third peak (indicated by the white arrow) is also present, coming from parts of the fiber in the transition. (b) Brillouin shift of two most prominent peaks as a function of sample temperature. The room temperature part of the fiber (red stars) is unaffected by the change in temperature. The temperature-varying peak (blue circles) crosses the 9.6 GHz point twice, at  $T = 191$  K and at  $T = 4$  K. (c) FWHM of the two most prominent peaks as a function of sample temperature. The room temperature part of the fiber (red stars) is unaffected by the change in temperature.

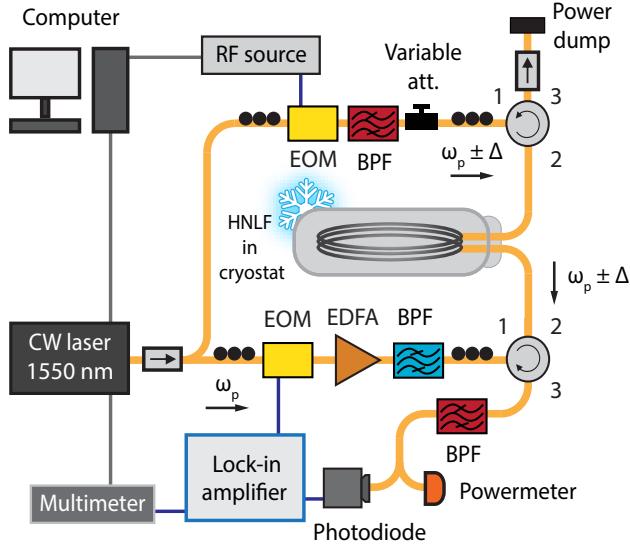


FIG. 10. **Pump-probe experiment.** Diagram of the setup used to measure Brillouin-Mandelstam scattering via a pump-probe experiment with lock-in amplifier detection. EOM: electro-optical modulator; Variable att.: variable attenuator; RF: radio frequency. The remaining abbreviations same as Fig. 6.

775

#### Pump-probe measurement

776 The setup used to perform the pump-probe experiment is shown in Fig. 10. The output of the laser described by  
 777 the previous section is divided into two paths, pump and probe. The light of the pump arm is modulated by  
 778 an electro-optical modulator (EOM) before amplification. The modulation frequency is given by a lock-in amplifier.  
 779 The light of the probe arm is modulated by an EOM connected to an RF source, generating thus two sidebands  
 780  $\omega_{\text{probe}} = \omega_{\text{pump}} \pm \Omega_B + \Delta_{\text{probe}}$ . These sidebands are swept around the resonance frequency  $\Omega_B$ . A narrowline  
 781 bandpass filter is placed after the EOM to select one sideband and probe only one of the Brillouin processes. The  
 782 light of each arm is coupled into the sample in opposite directions via circulators. To maximize the interaction between  
 783 the different waves, polarization controllers are placed on each arm. The port 3 of the probe circulator is connected  
 784 to an insulator followed by a power dump to get rid of the remaining pump light. The signal coming out of the port 3  
 785 of the pump circulator contains the probe frequency after the Brillouin interaction in the fiber plus the spontaneous  
 786 scattering generated by the pump. To decrease the noise in the measurement, the back-reflection is filtered by a  
 787 narrow bandpass filter. This signal is directed to a photodiode connected to the lock-in amplifier, where the resulting  
 788 electrical signal is demodulated to obtain the probe power as a function of time. The amplified electrical output of the  
 789 lock-in is measured by a multimeter. Both the RF-source and the multimeter are controlled by a computer, allowing  
 790 to measure the resulting Brillouin spectrum after the sweep without the need of a frequency reference. It was not  
 791 observed that the low power probe disturbs the strongly coupled system.

792

#### Temperature dependence of strong coupling threshold

793 As it was stated when describing the sample, we are able to reach the strong coupling regime thanks to the balance  
 794 of losses, Brillouin gain and power handling in our platform. Working at cryogenic temperature is beneficial, as  
 795 the acoustic dissipation rate ( $\Gamma_m$ ) decreases significantly and the Brillouin gain  $G_B$ , on which the effective coupling  
 796 strength depends, increases comparing to room temperature. Working at  $T = 4$  K, the lowest temperature accessible in  
 797 our experiment, proved to be our optimal point to perform strong coupling measurements (Fig. 11 (a)). A temperature  
 798 increase moves the system into the weak coupling regime. This can be seen in Fig. 11 (b) and (c), where the pump  
 799 power is the same as in (a), but the temperature is  $T = 10$  K and  $T = 19$  K, respectively. In these two cases, the  
 800 avoided crossing is less significant than at 4 K. The ideal working will differ in a different material and type of device.

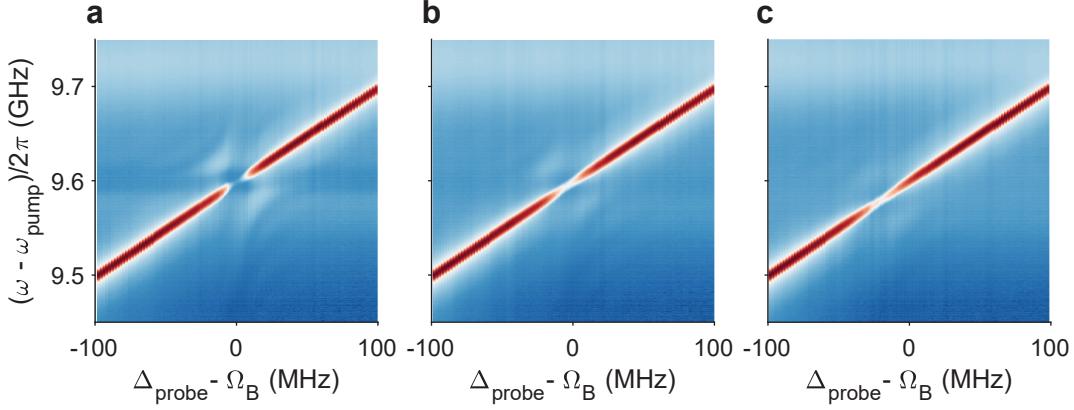


FIG. 11. **Temperature dependence of strong coupling regime.** (a) Forced detuning measurement at  $T = 4$  K,  $P_{\text{pump}} = 1.35 \pm 0.1$  W ( $g_{\text{om}} = 70 \pm 2$  MHz). As the system is in the strong coupling regime, it shows a clear avoided crossing. (b) Forced detuning measurement for  $T = 10$  K, same pump power as (a). The avoided crossing is not clearly visible, as the system enters the weak coupling regime. (c) Same as (b) with  $T = 19$  K.

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