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Supplementary Information for

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Sub-Diffraction Optical Confinement for Enhanced

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Second-Harmonic Generation in Suspended Thin-Film Lithium

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Niobate Nano-Cavity

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471 1. Electric field analysis of sub-diffraction suspended dielectric cavities

472 The suspended circular Bragg gratings are engineered with a tailored radial period to support
473 resonant operation across the 1250–1500 nm wavelength range. Starting from nonlinear Maxwell's
474 equations and assuming a time-harmonic electric field of the form $\mathbf{E}(\mathbf{r}, t) = \mathbf{E}(\mathbf{r})e^{-i\omega t}$.

475 In the absence of electrostatic interactions—that is, neglecting the free charge density ($\rho_f = 0$)
476 and the free current density ($\mathbf{J}_f = 0$)—the nonlinear Maxwell's equations can be simplified under
477 the high-frequency approximation (e.g., in the optical regime) as follows:

$$\nabla \cdot \mathbf{D} = 0$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} \quad (S1)$$

$$\nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t}$$

478 In Eqn. S1, \mathbf{D} and \mathbf{H} are electric displacement field and magnetic fields of the eigenmodes, respectively, and t represents time. The solution form of Maxwell's equations in cylindrical coordinates 480 is given in Eqn. S2.

$$\left[\frac{\partial^2}{\partial \rho^2} + \frac{1}{\rho} \frac{\partial}{\partial \rho} + \frac{1}{\rho^2} \frac{\partial^2}{\partial \varphi^2} \right] \mathbf{E}_j^{(\omega)} = -\mu_0 \omega^2 \mathbf{D}_j^{(\omega)} \quad (S2)$$

$$\left(\frac{\partial \mathbf{D}_z}{\partial \rho} + \frac{1}{\rho} \frac{\partial \mathbf{D}_y}{\partial \varphi} \right) \cos \varphi + \left(\frac{\partial \mathbf{D}_y}{\partial \rho} - \frac{1}{\rho} \frac{\partial \mathbf{D}_z}{\partial \varphi} \right) \sin \varphi = 0$$

481 Under the condition that only second-order nonlinear effects are considered, the components of 482 the electric displacement field can be described as D_x , D_y , and D_z , satisfying Eqn. S3.

$$\begin{pmatrix} \mathbf{D}_x \\ \mathbf{D}_y \\ \mathbf{D}_z \end{pmatrix} = \varepsilon_0 \begin{pmatrix} \varepsilon_{xx} & \varepsilon_{yx} & \varepsilon_{zx} \\ \varepsilon_{xy} & \varepsilon_{yy} & \varepsilon_{zy} \\ \varepsilon_{xz} & \varepsilon_{yz} & \varepsilon_{zz} \end{pmatrix} \begin{pmatrix} \mathbf{E}_x \\ \mathbf{E}_y \\ \mathbf{E}_z \end{pmatrix} + \varepsilon_0 \begin{pmatrix} \sum_{j,k} \chi_{xjk}^{(2)} \mathbf{E}_j \mathbf{E}_k \\ \sum_{j,k} \chi_{yjk}^{(2)} \mathbf{E}_j \mathbf{E}_k \\ \sum_{j,k} \chi_{zjk}^{(2)} \mathbf{E}_j \mathbf{E}_k \end{pmatrix} \quad (S3)$$

483 Lithium niobate is a negative uniaxial crystal (point group $3m$). Its linear dielectric tensor in 484 the crystal axis coordinate system is a diagonal matrix:

$$\boldsymbol{\varepsilon} = \begin{pmatrix} \varepsilon_{xx} & 0 & 0 \\ 0 & \varepsilon_{yy} & 0 \\ 0 & 0 & \varepsilon_{zz} \end{pmatrix} \quad (S4)$$

485 The last term in Eqn. S3 corresponds to the second-order nonlinear polarization, which can be 486 expressed as

$$\mathbf{P}_i^{(2)}(2\omega) = \varepsilon_0 \sum_{j,k} \chi_{ijk}^{(2)} \mathbf{E}_j(\omega) \mathbf{E}_k(\omega) \quad (S5)$$

487 where $\chi_{ijk}^{(2)}$ denotes the elements of the second-order nonlinear susceptibility tensor, and $\mathbf{E}_j(\omega)$, 488 $\mathbf{E}_k(\omega)$ are the components of the fundamental electric field at frequency ω .

$$\begin{pmatrix} \mathbf{P}_x^{(2)} \\ \mathbf{P}_y^{(2)} \\ \mathbf{P}_z^{(2)} \end{pmatrix} = 2\varepsilon_0 \begin{pmatrix} d_{11} & d_{21} & d_{31} & d_{14} & d_{15} & d_{16} \\ d_{12} & d_{22} & d_{32} & d_{24} & d_{25} & d_{26} \\ d_{13} & d_{23} & d_{33} & d_{34} & d_{35} & d_{36} \end{pmatrix} \begin{pmatrix} \mathbf{E}_x(\omega) \mathbf{E}_x(\omega) \\ \mathbf{E}_y(\omega) \mathbf{E}_y(\omega) \\ \mathbf{E}_z(\omega) \mathbf{E}_z(\omega) \\ 2\mathbf{E}_y(\omega) \mathbf{E}_z(\omega) \\ 2\mathbf{E}_x(\omega) \mathbf{E}_z(\omega) \\ 2\mathbf{E}_x(\omega) \mathbf{E}_y(\omega) \end{pmatrix} \quad (S6)$$

489 For lithium niobate (point group $3m$), the nonzero d components are:

$$d_{31} = d_{32} \neq 0, \quad d_{33} \neq 0, \quad d_{15} = d_{24} \neq 0 \quad (S7)$$

490 Therefore, the nonlinear polarization terms can be further simplified as:

$$\begin{aligned} \mathbf{P}_x^{(2)} &= 2d_{15}\mathbf{E}_y\mathbf{E}_z \\ \mathbf{P}_y^{(2)} &= 2d_{15}\mathbf{E}_x\mathbf{E}_z \\ \mathbf{P}_z^{(2)} &= d_{31}(\mathbf{E}_x^2 + \mathbf{E}_y^2) + d_{33}\mathbf{E}_z^2 \end{aligned} \quad (S8)$$

491 The substitution of Eqn. S8 into Eqn. S3 yields the nonlinear polarization component $[\mathbf{D}_x(\omega)$,

492 $\mathbf{D}_y(\omega), \mathbf{D}_z(\omega)$] as:

$$\begin{pmatrix} \mathbf{D}_x(\omega) \\ \mathbf{D}_y(\omega) \\ \mathbf{D}_z(\omega) \end{pmatrix} = \varepsilon_0 \begin{pmatrix} \varepsilon_{xx}(\omega)\mathbf{E}_x(\omega) + 2d_{15}\mathbf{E}_y(\omega)\mathbf{E}_z(\omega) \\ \varepsilon_{yy}(\omega)\mathbf{E}_y(\omega) + 2d_{15}\mathbf{E}_x(\omega)\mathbf{E}_z(\omega) \\ \varepsilon_{zz}(\omega)\mathbf{E}_z(\omega) + d_{31}(\mathbf{E}_x^2(\omega) + \mathbf{E}_y^2(\omega)) + d_{33}\mathbf{E}_z^2(\omega) \end{pmatrix} \quad (S9)$$

493 The second-order nonlinear optical effects are considered as higher-order perturbations in the

494 electromagnetic field analysis. Therefore, in this work, we assume the second-order nonlinear

495 susceptibility tensor components d_{33} , d_{31} , and d_{15} to be zero.

$$\begin{pmatrix} \mathbf{D}_x(\omega) \\ \mathbf{D}_y(\omega) \\ \mathbf{D}_z(\omega) \end{pmatrix} = \varepsilon_0 \begin{pmatrix} \varepsilon_{xx}(\omega)\mathbf{E}_x(\omega) \\ \varepsilon_{yy}(\omega)\mathbf{E}_y(\omega) \\ \varepsilon_{zz}(\omega)\mathbf{E}_z(\omega) \end{pmatrix} \quad (S10)$$

496 Substituting Eqn. S10 into Eqn. S2 yields Eqn. S11.

$$\begin{cases} \left[\frac{\partial^2}{\partial \rho^2} + \frac{1}{\rho} \frac{\partial}{\partial \rho} + \frac{1}{\rho^2} \frac{\partial^2}{\partial \varphi^2} \right] \mathbf{E}_i^{(\omega)} = -\frac{\omega^2}{c^2} n_{ii}^2(\omega) \mathbf{E}_i^{(\omega)} \\ \left[\frac{\partial}{\partial \rho} (n_{zz}^2(\omega) \mathbf{E}_z(\omega)) + \frac{1}{\rho} \frac{\partial}{\partial \varphi} (n_{yy}^2(\omega) \mathbf{E}_y(\omega)) \right] \cos \varphi \\ \quad + \left[\frac{\partial}{\partial \rho} (n_{yy}^2(\omega) \mathbf{E}_y(\omega)) - \frac{1}{\rho} \frac{\partial}{\partial \varphi} (n_{zz}^2(\omega) \mathbf{E}_z(\omega)) \right] \sin \varphi = 0 \end{cases} \quad (S11)$$

497 In the Eqn. S11, the anisotropic permittivity components $\varepsilon_{yy}(\omega)$ and $\varepsilon_{zz}(\omega)$ appear explicitly.

498 These can be equivalently expressed in terms of the refractive indices $n_{yy}(\omega)$ and $n_{zz}(\omega)$ via the

499 relation in Eqn. S12.

$$\varepsilon_{ii}(\omega) = n_{ii}^2(\omega), \quad i = x, y, z \quad (S12)$$

500 We assume that each component of the electric field can be expressed in a separable form as

$$E_i^{(\omega)}(\rho, \varphi) = R_i(\rho) \Phi_i(\varphi) \quad (S13)$$

501 where $R_i(\rho)$ and $\Phi_i(\varphi)$ represent the radial and angular components of the electric field, respec-
502 tively. Due to the inherent periodicity of the angular coordinate φ (with period 2π), the angular
503 function $\Phi_i(\varphi)$ is chosen as

$$\Phi_i(\varphi) = e^{im_i\varphi}, \quad m_i \in \mathbb{Z} \quad (S14)$$

504 where m_i is an integer ensuring the single-valuedness and periodicity of the wavefunction. Substi-
505 tuting the separated variables into the first equation yields

$$\frac{1}{R_i} \left(\frac{d^2 R_i}{d\rho^2} + \frac{1}{\rho} \frac{dR_i}{d\rho} \right) - \frac{m_i^2}{\rho^2} = -\frac{\omega^2}{c^2} n_{ii}^2(\omega) \quad (S15)$$

506 By algebraic manipulation, we obtain the radial differential equation

$$\frac{d^2 R_i}{d\rho^2} + \frac{1}{\rho} \frac{dR_i}{d\rho} + \left[k_i^2 - \frac{m_i^2}{\rho^2} \right] R_i = 0 \quad (S16)$$

507 where

$$k_i = \frac{\omega}{c} n_{ii}(\omega) \quad (S17)$$

508 Eqn. S16 is the standard Bessel equation, whose general solution can be expressed as a linear
509 combination of Bessel functions:

$$R_i(\rho) = A_i J_{m_i}(k_i \rho) + B_i Y_{m_i}(k_i \rho) \quad (S18)$$

510 where $J_{m_i}(k_i \rho)$ is the first kind Bessel function, and $Y_{m_i}(k_i \rho)$ is the second kind Bessel function
511 (also known as the Neumann function). The constants A_i and B_i are determined by boundary
512 conditions.

513 **Regular case without singularities.** In typical cylindrical geometries where the domain includes
514 the origin ($\rho = 0$) and no geometric singularity is present, the solution to the radial equation must
515 be finite at $\rho = 0$. Since the second kind Bessel function, $Y_{m_i}(k_i \rho)$, diverges at the origin, the

516 physical requirement of regularity demands that its contribution be excluded. Thus, the general
517 solution simplifies to:

$$R_i(\rho) = A_i J_{m_i}(k_i \rho) \quad (S19)$$

518 where A_i is a constant determined by boundary conditions. In this case, the electric field remains
519 finite.

520 **Case with bowtie-shaped singularities.** In contrast, when a bowtie-shaped singularity—such as
521 a sharp metallic tip or a subwavelength dielectric gap—is present near or at $\rho = 0$, the center is no
522 longer a regular point in the domain. Such geometric features introduce a physical or mathematical
523 singularity that invalidates the regularity condition at the origin.

524 In this scenario, the solution to the radial equation must retain both Bessel functions:

$$R_i(\rho) = A_i J_{m_i}(k_i \rho) + B_i Y_{m_i}(k_i \rho) \quad (S20)$$

525 where B_i takes nonzero values depending on the field behavior near the singularity. The divergent
526 nature of Y_{m_i} at the origin is no longer unphysical, but may reflect genuine field enhancement
527 arising from the singular structure. Such effects are particularly significant in dielectric nanogaps
528 or nonlinear optical hotspots, where geometric singularities lead to localized field amplification.
529 The higher-order small terms of the electric field can be neglected, and the eigenmodes **E** and **H**
530 can be expressed in Eqn. [S21](#).

$$\begin{aligned}
\mathbf{E}_y &= \begin{cases} \frac{\alpha}{\varepsilon_{yy}} C(k_0 \rho)^{-l} \cos[l\varphi], & -\frac{\theta}{2} \leq \varphi \leq \frac{\theta}{2} \\ \frac{\alpha}{\varepsilon_{yy}} C(k_0 \rho)^{-l} \cos[l(\pi - \varphi)], & \pi - \frac{\theta}{2} \leq \varphi \leq \pi + \frac{\theta}{2} \\ C(k_0 \rho)^{-l} \cos[l(\frac{\pi}{2} + \varphi)], & -\pi + \frac{\theta}{2} < \varphi < -\frac{\theta}{2} \\ C(k_0 \rho)^{-l} \cos[l(\frac{\pi}{2} - \varphi)], & \frac{\theta}{2} < \varphi < \pi - \frac{\theta}{2} \\ \frac{\alpha}{\varepsilon_{zz}} C(k_0 \rho)^{-l} \sin[l\varphi], & -\frac{\theta}{2} \leq \varphi \leq \frac{\theta}{2} \end{cases} \\
\mathbf{E}_z &= \begin{cases} -\frac{\alpha}{\varepsilon_{zz}} C(k_0 \rho)^{-l} \sin[l(\pi - \varphi)], & \pi - \frac{\theta}{2} \leq \varphi \leq \pi + \frac{\theta}{2} \\ C(k_0 \rho)^{-l} \sin[l(\frac{\pi}{2} + \varphi)], & -\pi + \frac{\theta}{2} < \varphi < -\frac{\theta}{2} \\ -C(k_0 \rho)^{-l} \sin[l(\frac{\pi}{2} - \varphi)], & \frac{\theta}{2} < \varphi < \pi - \frac{\theta}{2} \end{cases} \\
\mathbf{E}_x &= 0 \\
\mathbf{H}_x &= \mathbf{H}_y = \mathbf{H}_z = 0
\end{aligned} \tag{S21}$$

531 The analytical solution suggests an infinite electric field intensity at the hotspot. Nevertheless,
532 due to the impossibility of a zero gap distance in real structures, the field enhancement factor is
533 ultimately finite.

534 2. Nonlinear coupling wave equation and SHG enhancement

535 In the absence of losses and under the slowly varying envelope approximation, the nonlinear coupled
536 wave equations in the time-domain electromagnetic field can be expressed as shown in Eqn. S22.

$$\begin{cases} \frac{d\tilde{\alpha}_1}{dt} = -i\beta_1 \tilde{\alpha}_1^* \tilde{\alpha}_2 e^{-i(\omega_2 - 2\omega_1)t} \\ \frac{d\tilde{\alpha}_2}{dt} = i\beta_2 \tilde{\alpha}_1^2 e^{-i(2\omega_1 - \omega_2)t} \end{cases} \tag{S22}$$

537 In Eqn. (S22), $\tilde{\alpha}_1$ and $\tilde{\alpha}_2$ denote the complex slowly varying amplitudes of the coupled waves
538 at frequencies ω_1 and ω_2 , respectively, g represents the nonlinear coupling coefficient, ω_1 and ω_2
539 are the angular frequencies of the modes, the asterisk $*$ denotes the complex conjugate.

540 Taking into account losses and input excitation, the nonlinear coupled wave equations are given
 541 in Eqn. S23.

$$\begin{cases} \frac{d\tilde{\alpha}_1}{dt} = -\frac{\kappa_{10} + \kappa_{1e}}{2}\tilde{\alpha}_1 + \sqrt{\kappa_{1e}}s e^{-i(\omega_p - \omega_1)t} - i\beta_1 \tilde{\alpha}_1^* \tilde{\alpha}_2 e^{-i(\omega_2 - 2\omega_1)t} \\ \frac{d\tilde{\alpha}_2}{dt} = -\frac{\kappa_{20} + \kappa_{2e}}{2}\tilde{\alpha}_2 + i\beta_2 \tilde{\alpha}_1^2 e^{-i(2\omega_1 - \omega_2)t} \end{cases} \quad (\text{S23})$$

542 where ω_p and s denote the frequency and the amplitude of the input electric field in the pump fibre,
 543 with $|s|^2$ being the input power, κ_{j0} and κ_{je} represent the intrinsic decay rate and external coupling
 544 rate, respectively. Under the assumption of solely second-order nonlinear effects, the nonlinear
 545 coupling coefficients β_1 and β_2 are defined as presented in Eqn. S24⁴⁵.

$$\begin{cases} \beta_1 = \frac{1}{4} \frac{\int d^3x \sum_{ijk} \varepsilon \chi_{ijk}^{(2)} (\mathbf{E}_{1i}^* \mathbf{E}_{2j} \mathbf{E}_{1k}^* + \mathbf{E}_{1j}^* \mathbf{E}_{2k} \mathbf{E}_{1i}^*)}{(\int d^3x \varepsilon |\mathbf{E}_1|^2) (\int d^3x \varepsilon |\mathbf{E}_2|^2)^{1/2}} \\ \beta_2 = \frac{1}{4} \frac{\int d^3x \sum_{ijk} \varepsilon \chi_{ijk}^{(2)} \mathbf{E}_{2i}^* \mathbf{E}_{1j} \mathbf{E}_{1k}}{(\int d^3x \varepsilon |\mathbf{E}_1|^2) (\int d^3x \varepsilon |\mathbf{E}_2|^2)^{1/2}} \end{cases} \quad (\text{S24})$$

546 In the rotating frame of the pump, $\alpha_1 = \tilde{\alpha}_1 e^{i(\omega_p - \omega_1)t}$ and $\alpha_2 = \tilde{\alpha}_2 e^{i(2\omega_p - \omega_2)t}$, the coupled wave
 547 equations can be expressed in Eqn. S25.

$$\begin{cases} \frac{d\alpha_1}{dt} = \left[i(\omega_p - \omega_1) - \frac{\kappa_{10} + \kappa_{1e}}{2} \right] \alpha_1 + \sqrt{\kappa_{1e}}s - i\beta_1 \alpha_1^* \alpha_2 \\ \frac{d\alpha_2}{dt} = \left[i(2\omega_p - \omega_2) - \frac{\kappa_{20} + \kappa_{2e}}{2} \right] \alpha_2 + i\beta_2 \alpha_1^2 \end{cases} \quad (\text{S25})$$

548 The pump is almost unperturbed by SHG, since the pump light is much stronger than the SH
 549 signal. Therefore, the last term in Eqn. S25 can be ignored in the following analysis. Considering
 550 the steady state, i.e., $\frac{d\tilde{\alpha}_1}{dt} = \frac{d\tilde{\alpha}_2}{dt} = 0$, the above coupled mode equations result in the expression of
 551 generated SH power⁴⁶,

$$P_2 = \frac{4|\beta|^2 Q_2^2}{\omega_2 Q_{2e} \left[4Q_2^2 \left(\frac{2\omega_p}{\omega_2} - 1 \right)^2 + 1 \right]} \cdot \frac{16Q_1^4}{Q_{1e}^2 \omega_1^2 \left[4Q_1^2 \left(\frac{\omega_p}{\omega_1} - 1 \right)^2 + 1 \right]^2} P_1^2 \quad (\text{S26})$$

552 Here, $Q_j = \frac{\omega_j}{\kappa_{j0} + \kappa_{je}}$ and $Q_{je} = \frac{\omega_j}{\kappa_{je}}$ denote the loaded quality factor and the external (coupling-
 553 induced) quality factor, respectively. Under the phase-matching condition, i.e., $\omega_p = \omega_1 = \omega_2/2$,
 554 and assuming critical coupling ($Q_j = Q_{je}$), the conversion efficiency scales as $\frac{P_2}{P_1^2} \propto Q_2 Q_1^2 |\beta|^2$.

555 From Eqn. S24, we can derive the relationship between the mode volume V_m and the coupling
556 coefficients. In this case, any integral over the fields will simply yield the mode volume V_m of the
557 nonlinear material. Thus, for the $\chi^{(2)}$ effect, we obtain $\beta_i \sim g \frac{\chi^{(2)}}{\sqrt{V_m}}$, where g represents the coupling
558 coefficient into the cavity. In fact, although the calculated mode volume is very small, the overall
559 enhancement factor does not increase significantly because the coupling coefficient between the
560 Gaussian beam and the nanocavity is quite small, resulting in a relatively small value of g .

561 **3. Fabrication of suspended CBGs and bowtie structures in suspended CBG**

562 The fabrication process of the suspended CBG structure with an integrated bowtie consists of
563 several steps, as illustrated in Fig. S1. Firstly, a 600-nm-thick amorphous silicon is deposited on
564 the TFLN wafer via plasma-enhanced chemical vapor deposition (PECVD), followed by spin-
565 coating of ZEP520A electron beam resist. The designed patterns are then exposed by electron beam
566 lithography and developed by pentyl acetate. Subsequently, the pattern is transferred to the silicon
567 layer using inductively coupled plasma reactive ion etching (ICP-RIE). The underlying TFLN is
568 further etched via ICP to form the nanostructures. Afterward, the silicon hard mask is removed,
569 and selective wet etching of the buried SiO_2 layer is performed to release the suspended structure.

570 **4. Experimental setup for reflection measurement**

571 As shown in Fig. S2, the light source is a picosecond supercontinuum laser with a pulse duration
572 of 220 ps (YSL photonics SC-pro, repetition rate: 20 MHz). The supercontinuum is firstly filtered
573 by a long-pass filter (>1250 nm). The input light is then tightly focused on the sample by a NIR
574 microscope objective (Mitutoyo 50 \times , NA = 0.65). Reflection light is collected by the same objective
575 and reflected by a beam splitter (50:50, 600–1700 nm). A flip mirror is added after the beam splitter
576 to guide the beam into two arms. The light is either coupled into a multimode fiber and recorded
577 by a spectrometer (Anritsu, MS9740A) or imaged using a camera (EMCCD, iXon Ultra 897).

578 **5. Experimental setup for SHG enhancement**

579 As shown in Fig. S3, during the SHG signal measurement, the supercontinuum source is spectrally
580 filtered using a tunable high-power filter (YSL Photonics AOTF-PRO2, FWHM 1.9 nm). The

581 output beam then passes through a Glan prism and half-wave plate (@1310 nm) to adjust the
582 polarization of the excitation light. Afterward, the beam is directed through two beam splitters (BS)
583 and a microscope objective, tightly focused onto the center of the sample. The reflected signal is
584 redirected by the same plate beam splitter to a EMCCD camera (iXon Ultra 897) for measuring the
585 SHG intensity of the sample, or alternatively, coupled into a spectrometer (Ocean Optics, HR4000)
586 via a fiber coupling system to analyze the SHG spectrum.

587 **6. Design of suspended CBGs and bowtie structures in suspended CBG**

588 The sample is simulated using the finite-difference time-domain (FDTD) method. To enhance the
589 refractive index contrast, suspended supports are designed within the circular Bragg cavity, as
590 shown in Fig. S4. The size of the supporting structures is minimized—down to 90 nm—to ensure
591 sufficient mechanical stability while preventing the collapse of the sample.

592 By tuning the period and duty cycle of the sample, different resonant structures can be engi-
593 neered. Using the FDTD method, structures with periods ranging from 720 to 840 nm and duty
594 cycles between 0.58 and 0.66 are designed. The resonance wavelength can be shifted by adjusting
595 the period (Fig. S5-S8). Considering that the etching angle depends on both the grating period and
596 duty cycle, the designed resonances are centered at around 1310 nm.

597 **7. Discussion of electric field distributions of bowtie with different gap sizes**

598 The electric field distribution within the bowtie structure is strongly influenced by the gap size. As
599 the gap narrows, the electromagnetic coupling between the two dielectric tips intensifies, leading to
600 a significant increase in the local field enhancement at the dielectric gap (Fig. S9). This enhanced
601 confinement can greatly improve nonlinear optical effects like SHG.

602 However, reducing the gap size also presents fabrication challenges and may introduce additional
603 losses or scattering due to imperfections. The field confinement becomes more spatially localized
604 in smaller gaps, requiring high fabrication precision to fully utilize the enhancement. In our work,
605 the fabrication limit of the gap size is 20 nm (Fig. S10).

606 **8. Discussion of related work**

607 Bowtie nanostructure integrated within a suspended circular Bragg cavity has been experimentally
608 and theoretically designed, enabling giant SHG enhancement beyond the diffraction limit. The
609 information of the fundamental and second harmonic signals is shown in Tables [S1](#) and [S2](#). The
610 CBG nanocavity achieves a high normalized conversion efficiency of $0.85 \times 10^{-2} \text{ cm}^2/\text{GW}$ under
611 a pump intensity of 1 MW/cm^2 , with a mode volume as small as $7.58 \times 10^{-4} (\lambda/n)^3$. An SHG
612 enhancement factor of 3,720 is achieved compared to bare TFLN. Efficient SHG under ultralow
613 pump intensities is also demonstrated, significantly improving both the device performance and
614 operational lifetime, while simultaneously reducing the mode volume.

615 In contrast to plasmonic resonances, the bowtie-integrated CBG structure is free from thermal
616 losses and supports higher optical powers, significantly extending the upper limit of nonlinear
617 conversion efficiency while maintaining an ultrasmall mode volume. Furthermore, compared to
618 other all-dielectric nanostructures, our design exhibits a significantly reduced mode volume while
619 maintaining a high SHG efficiency. The comparison is shown in Fig. [5H](#) and Table [S3](#). Notably,
620 this work represents the first experimental realization of a nonlinear optical response beyond the
621 diffraction limit in a all-dielectric nanocavity.

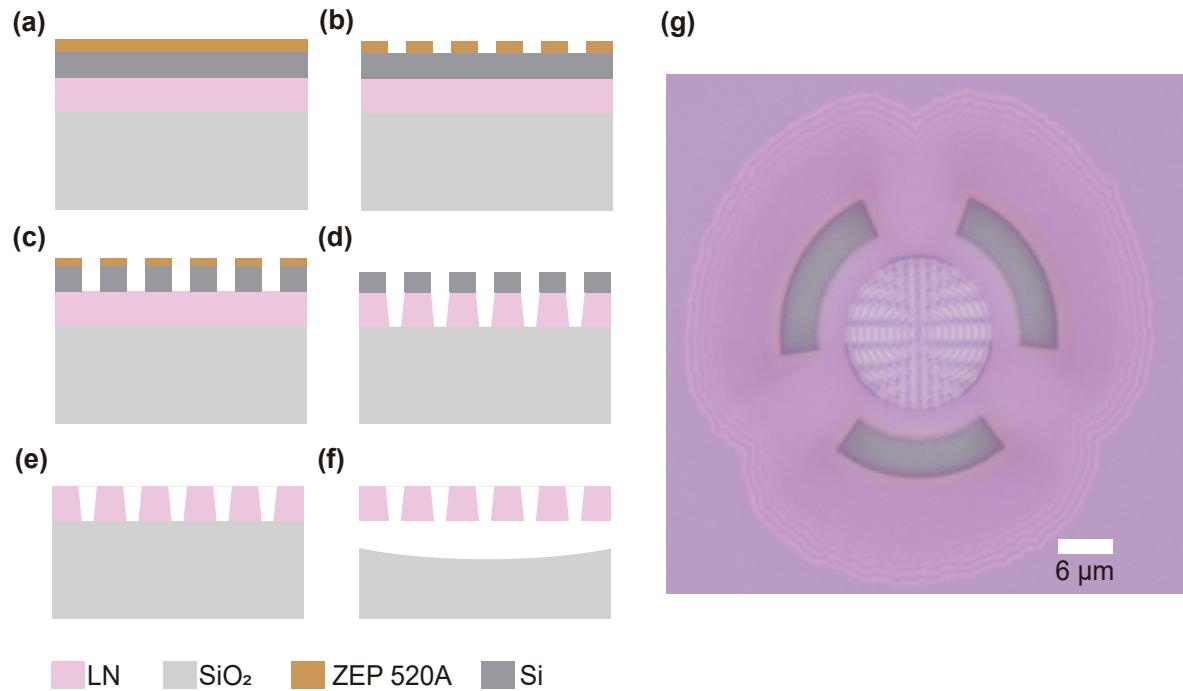


Figure S1: Fabrication flowchart of the sample. (a) Deposition of 600-nm amorphous silicon on TFLN via PECVD, followed by spin coating of ZEP520A photoresist. (b) Electron beam exposure and development. (c) ICP-RIE etching of silicon mask. (d) RIE etching of LN. (e) Removal of silicon. (f) Selective etching of silicon dioxide. (g) Optical microscope image of the sample.

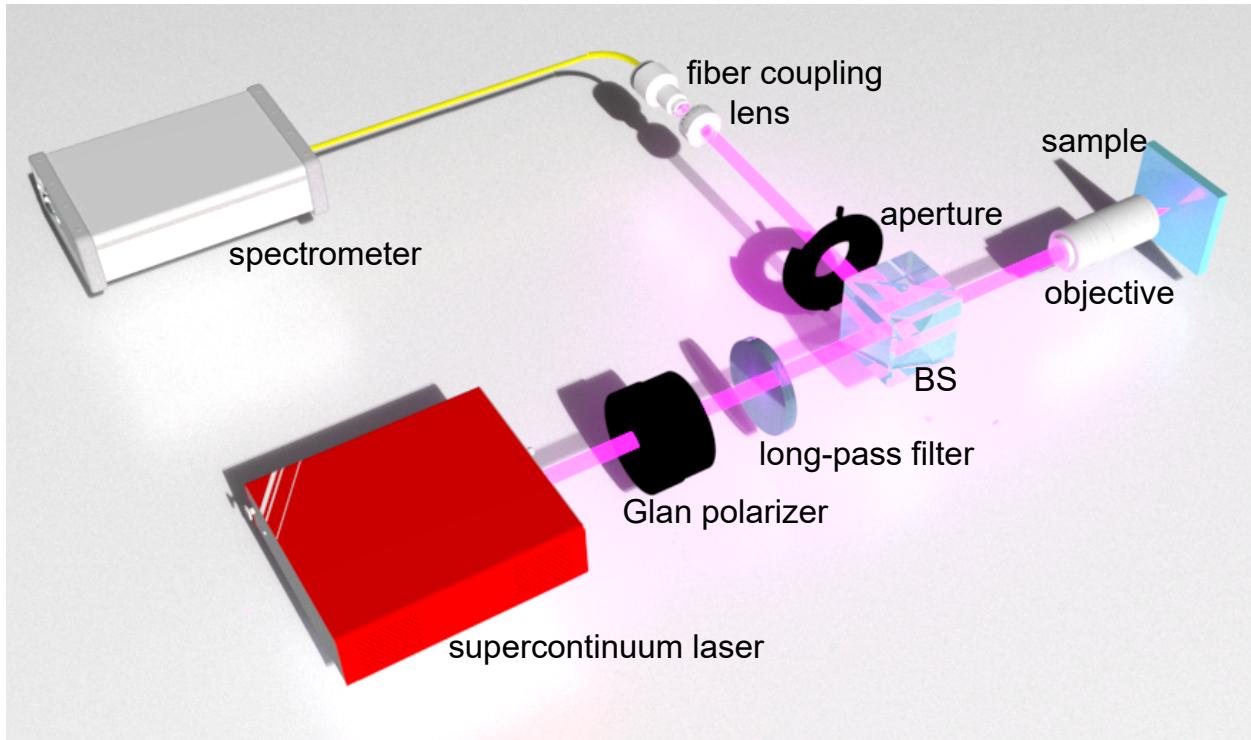


Figure S2: Experimental setup for reflection measurement. The supercontinuum laser (YSL photonics SC-pro, 430–2400 nm) passes a Glan polarizer for polarization control. Then, it is filtered by a long-pass filter (>1250 nm), to avoid the intense seed at 1064 nm. The input light is then tightly focused on the sample by a NIR microscope objective (Mitutoyo, 50 \times , NA=0.65). The reflection signal is collected by the same objective and reflected by a beam splitter (50:50, 600–1700 nm). The reflection signal is coupled into a single-mode optical fiber (the coupling efficiency is 30%) and recorded by a spectrometer (Anritsu, MS9740A).

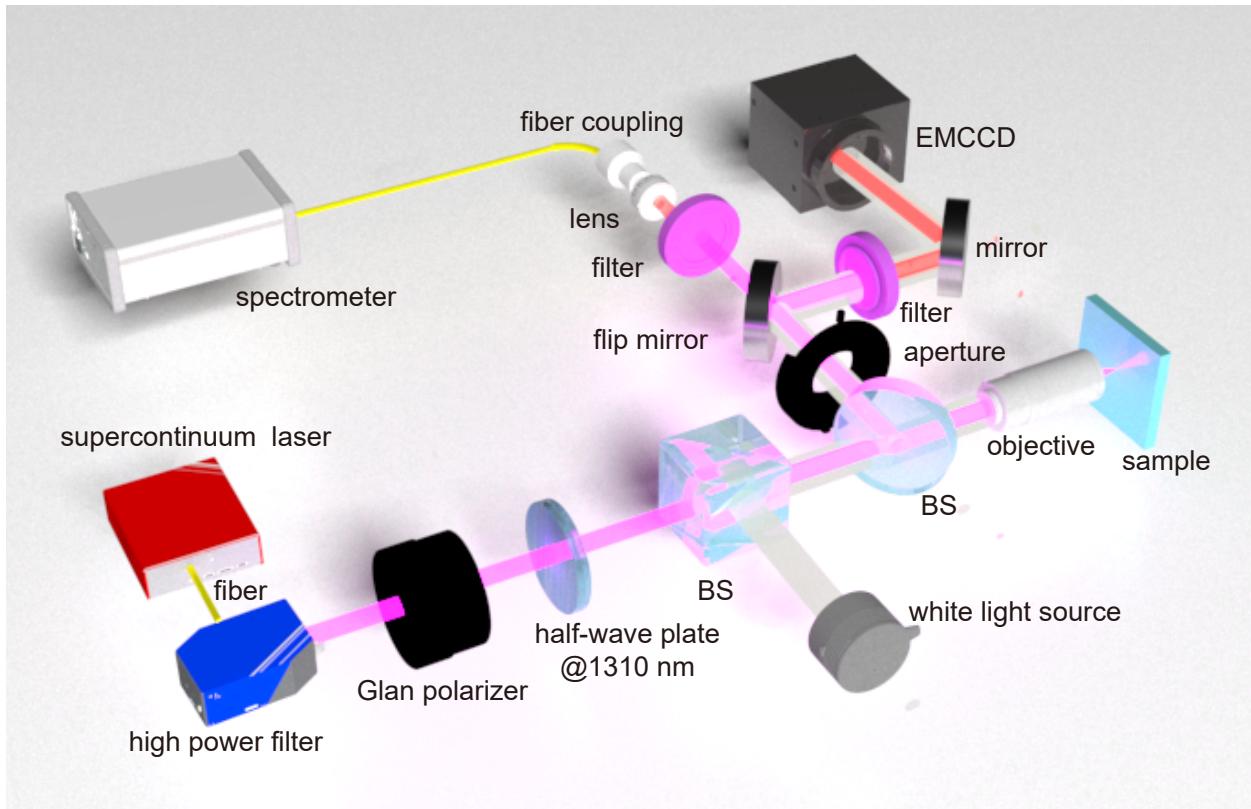


Figure S3: Experimental setup for SHG enhancement. During the SHG signal measurement, the supercontinuum source is spectrally filtered using a tunable high-power filter (YSL Photonics AOTF-PRO2, FWHM 1.9 nm). The output beam then passes through a Glan prism and half-wave plate (@1310 nm) to adjust the polarization of the excitation light. Afterward, the beam is directed through two beam splitters (BS) and a microscope objective, tightly focused onto the center of the sample. The reflected signal is redirected by the same plate beam splitter to a EMCCD camera (iXon Ultra 897) for measuring the SHG intensity of the sample, or alternatively, coupled into a spectrometer (Ocean Optics, HR4000) via a fiber coupling system to analyze the SHG spectrum.

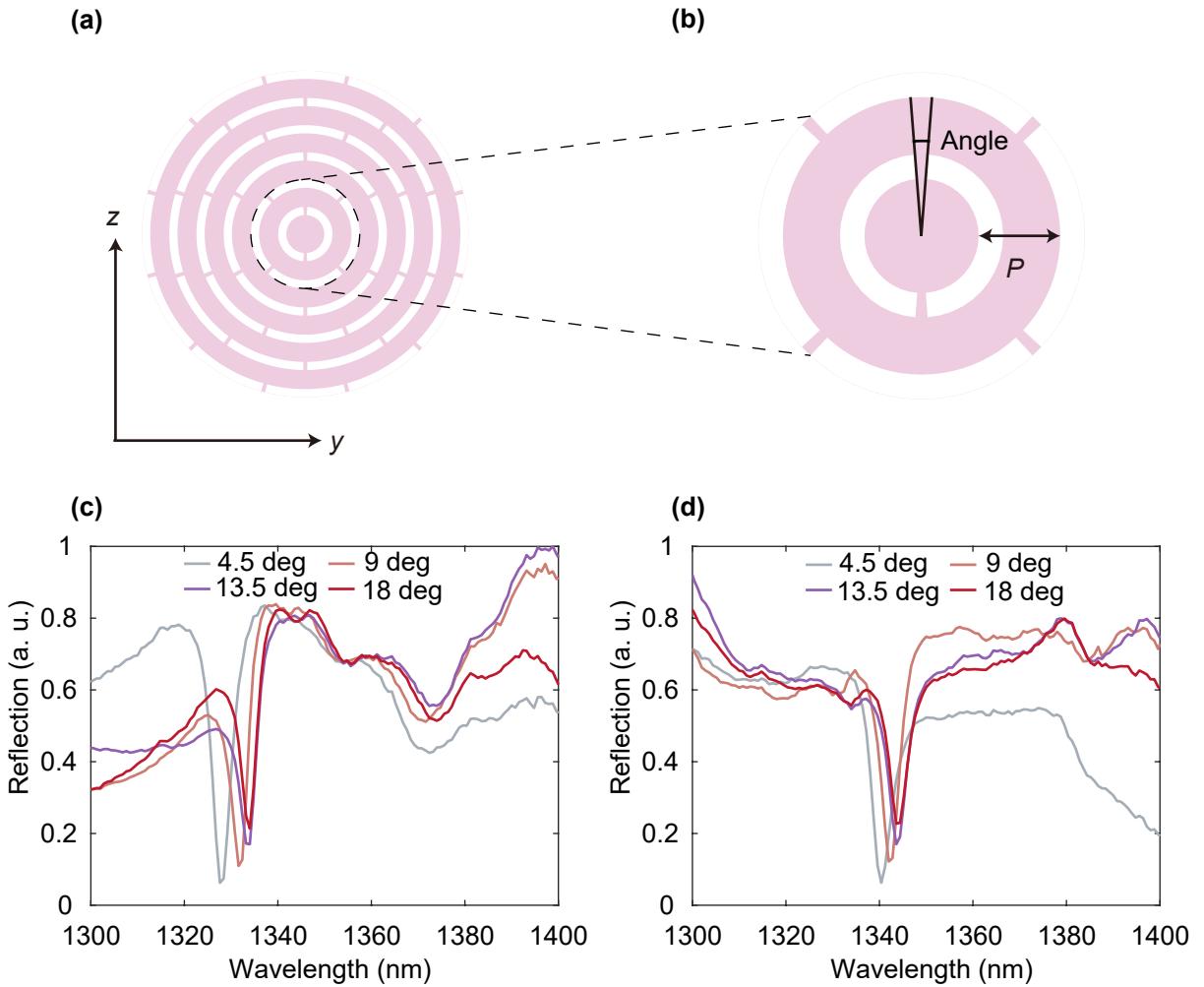


Figure S4: Influence of the width of the suspended supports on the resonance. (a and b)
 Schematics of the suspended supports in the CBG, illustrating that smaller angles correspond to reduced support size. **(c and d)** Reflection spectra under z-polarized and y-polarized pump excitation. A decrease in angle leads to an increased Q factor.

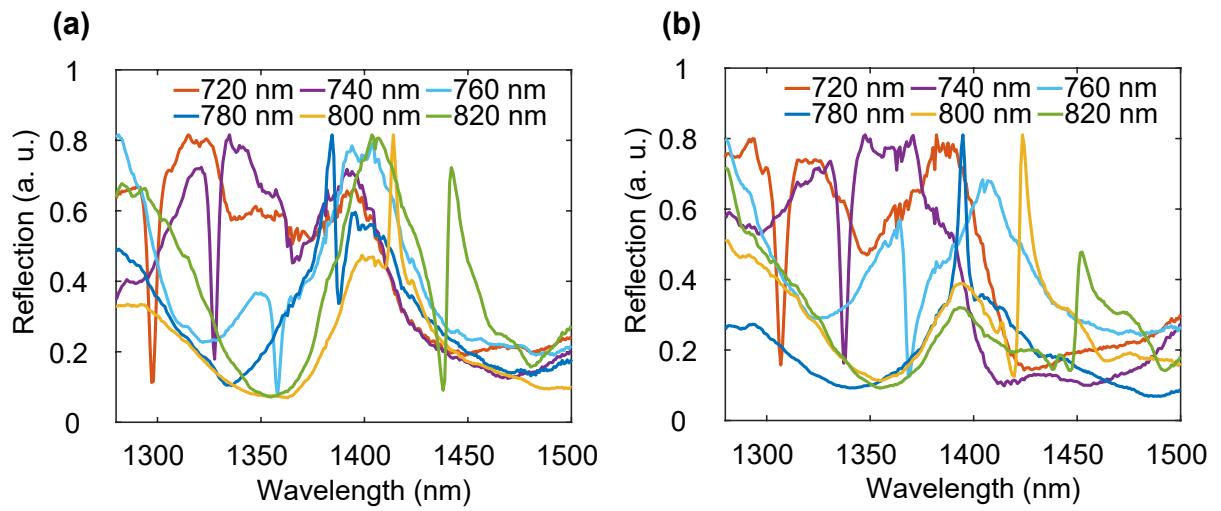


Figure S5: Experimental reflection spectra of suspended CBGs with different P values under (a) z-polarized and (b) y-polarized illumination.

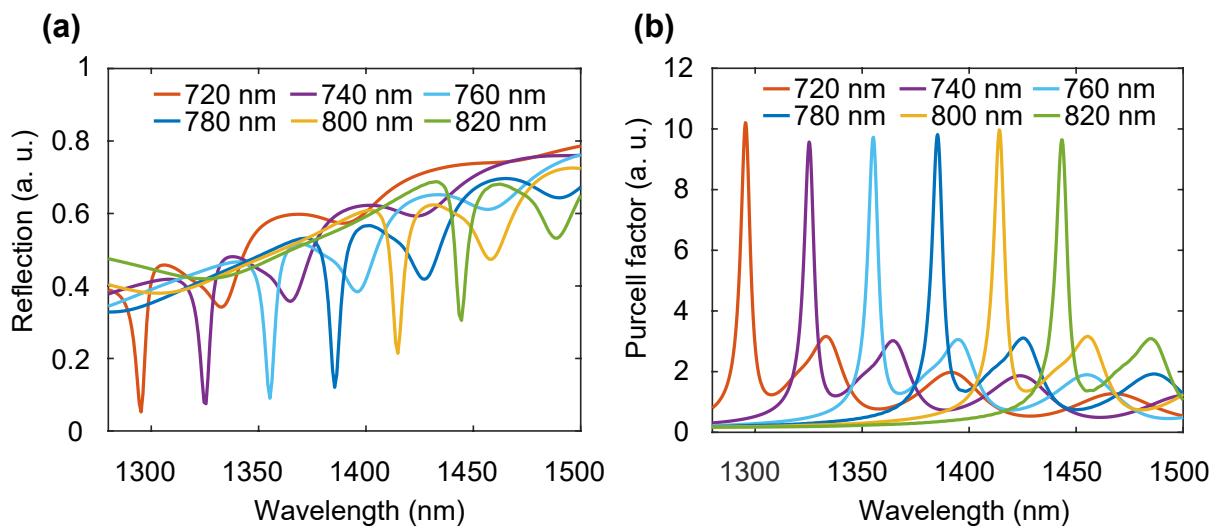


Figure S6: (a) Simulated reflection spectra of the suspended CBG under z-polarized illumination and (b) the corresponding Purcell factors.

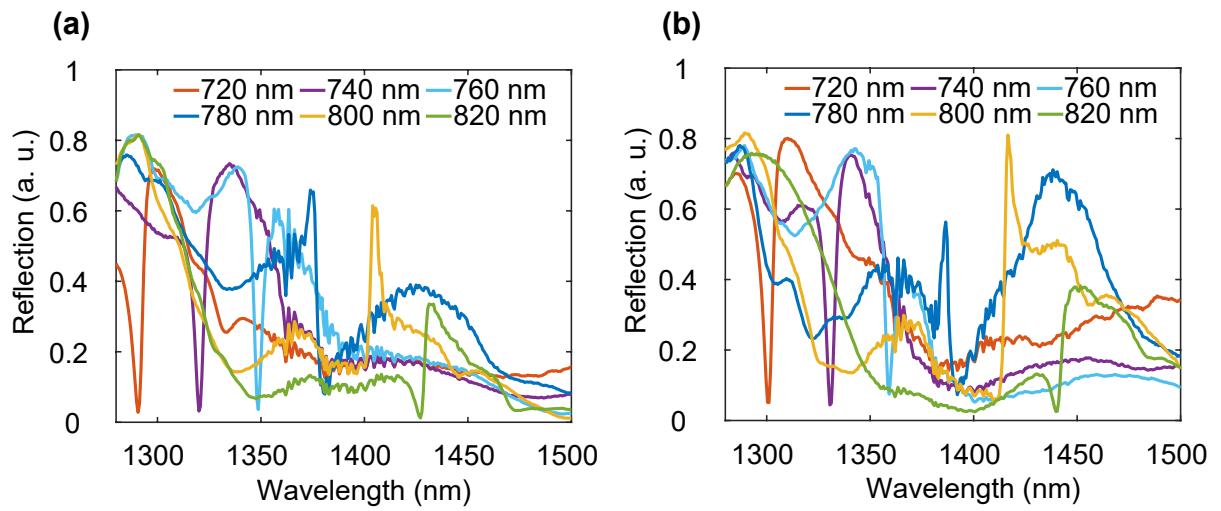


Figure S7: Experimental reflection spectra of bowtie in suspended CBG with different P 's under (a) z-polarized and (b) y-polarized illumination.

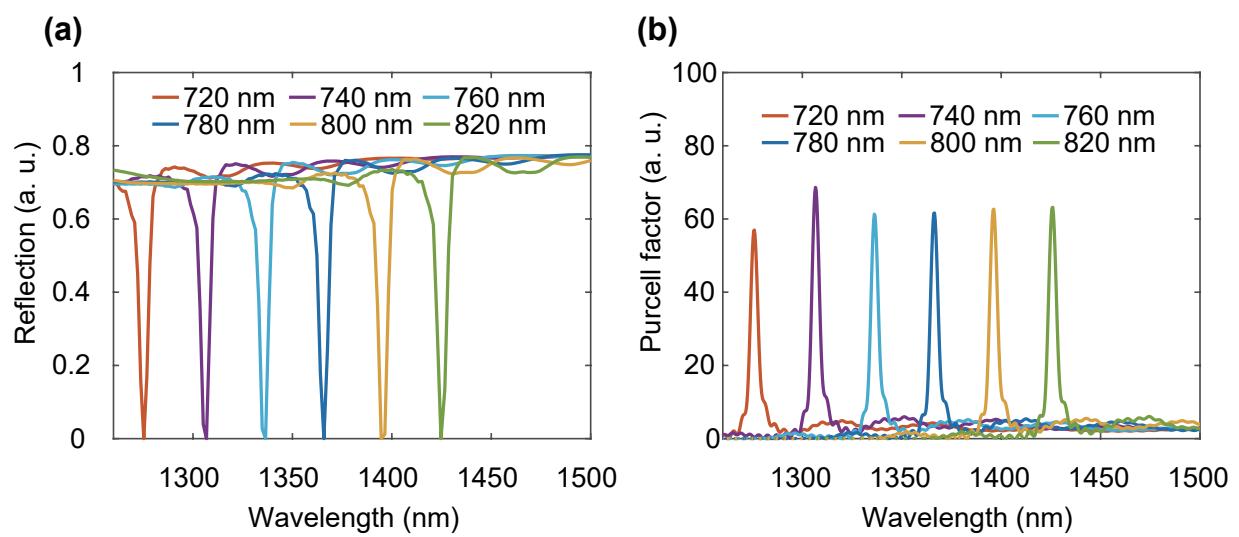


Figure S8: (a) Simulated reflection spectra of the bowtie in suspended CBG under z-polarized illumination and (b) the corresponding Purcell factors.

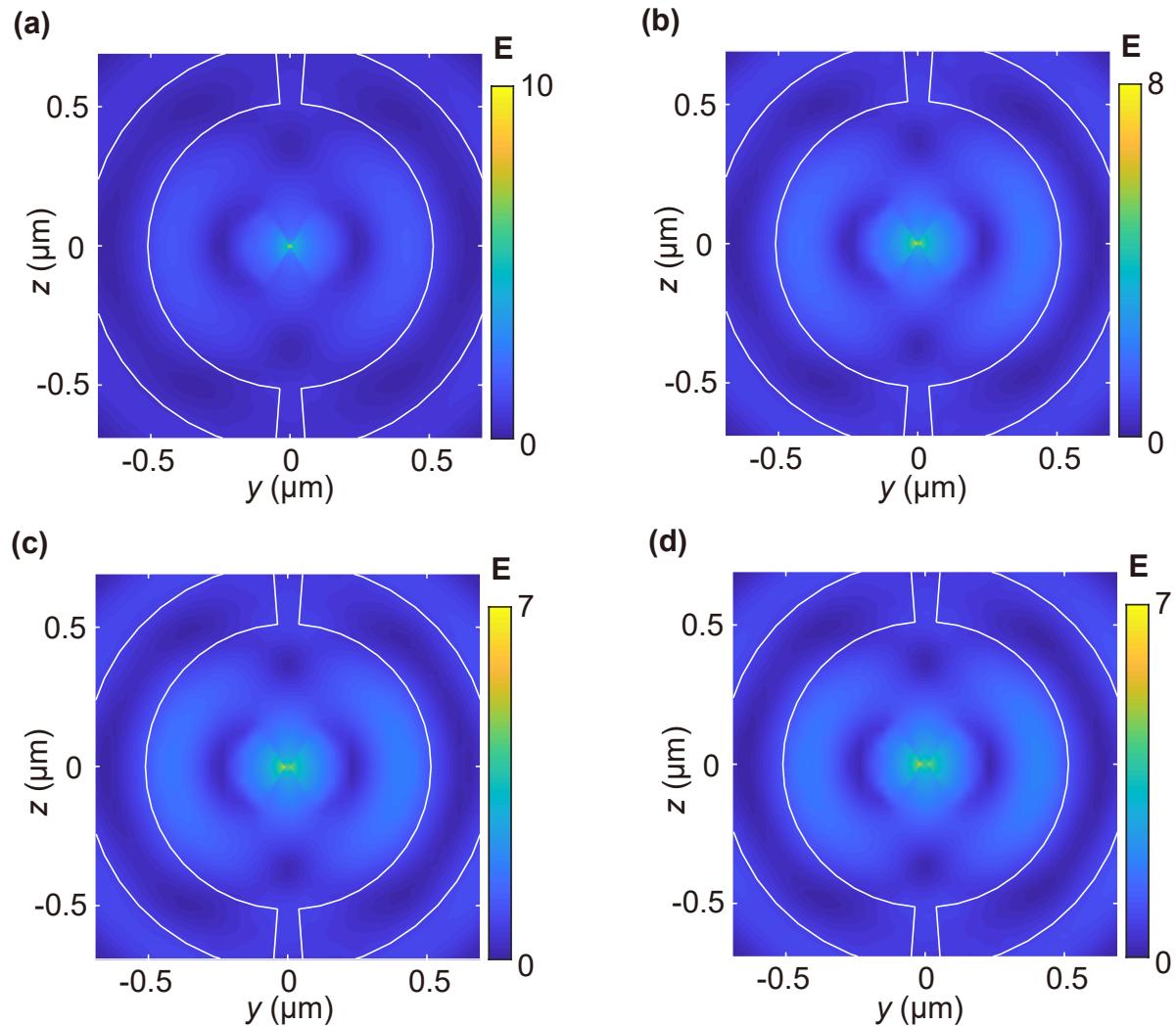


Figure S9: Simulated electric field distributions of the bowtie in suspended CBG structures with gap sizes of **(a)** 0 nm, **(b)** 10 nm, **(c)** 20 nm, and **(d)** 30 nm.

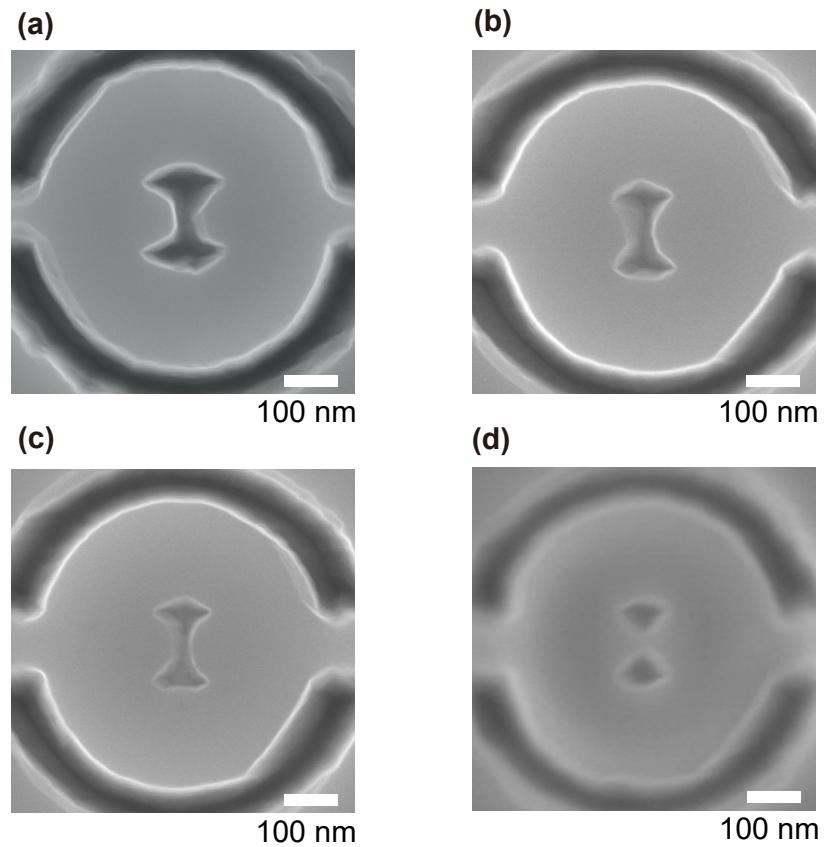


Figure S10: The fabricated sample is designed with a minimum gap of 20 nm. Due to the inclined etching angle, the actual separation at the tip of the sloped sidewalls is effectively reduced to 0 nm.

Table S1: Experimental parameters and input power levels. The table lists the laser excitation parameters, including wavelength, repetition rate, and pulse width, as well as the calculated spot diameter and peak power.

Parameter	Wavelength	Rep. rate	Pulse length	Avg. power	NA	Spot diameter	Peak power
	(nm)	(MHz)	(ps)	(mW)	–	(μm)	(mW)
Symbol	λ	ν	τ	P_{FH}	–	δ	\hat{P}_{FH}
Formula	N/A	N/A	N/A	N/A	N/A	$\frac{1.22\lambda}{\text{NA}}$	$\frac{P_{\text{FH}}}{\nu\tau}$
Value	1310	20	220	0.21	0.65	2.46	47.7

Table S2: SHG conversion efficiency The table lists SHG related parameters in our experiment including SHG power, peak power, conversion efficiency, peak SHG efficiency, and normalized efficiency.

Parameter	SHG Power	SHG Peak Power	Max. conv. eff.	Peak SHG eff.	Normalized SHG eff.
	(nW)	(W)	–	(W^{-1})	(cm^2/GW)
Symbol	P_{SH}	\hat{P}_{SH}	η_{SHG}	γ_{SHG}	η_{norm}
Formula	$N \cdot E_{\text{ph}}$	$\frac{\hat{P}_{\text{SH}}}{\nu\tau}$	$\frac{P_{\text{SH}}}{P_{\text{FH}}}$	$\frac{\hat{P}_{\text{SH}}}{\hat{P}_{\text{FH}}^2}$	$\frac{\eta_{\text{SHG}} \cdot \pi \left(\frac{\delta}{2}\right)^2}{\hat{P}_{\text{FH}}}$
Value	1.8	4.09×10^{-7}	8.6×10^{-6}	1.78×10^{-4}	0.85×10^{-2}

Table S3: Comparison of nonlinear optical performance across nanophotonic platforms. This table compares the Q factor, mode volume, SHG efficiency, and normalized SHG efficiency of various reported nanophotonic resonators.

Type	Q factor	Mode volume (λ/n) ³	Wavelength (nm)	SHG efficiency	Norm. SHG efficiency (cm ² /GW)	Reference
This work	~370	7.58×10^{-4}	1310	8.6×10^{-6}	0.85×10^{-2}	N/A
Plasmonic	~20	6.45×10^{-6}	1550	6.4×10^{-9}	7.88×10^{-9}	Nat. Nanotechnol. 10 , 412 (2015) ¹⁰
Plasmonic	~10	1.63×10^{-7}	850	0.87×10^{-6}	9.92×10^{-8}	Nat. Commun. 12 , 4326 (2021) ¹⁴
Plasmonic	~30	6×10^{-6}	1560	1.3×10^{-7}	1.23×10^{-7}	Opt. Express 32 , 13140 (2024) ¹⁵
Plasmonic	~10	1.3×10^{-7}	1560	N/A	N/A	Nano Lett. 15 , 4102 (2015) ¹¹
Plasmonic	~5	5×10^{-2}	650	3.7×10^{-12}	2.8×10^{-13}	Light Sci. Appl. 7 , 49 (2018) ¹⁶
Plasmonic	N/A	5×10^{-4}	800–1300	1.13×10^{-6}	1.29×10^{-7}	Nat. Commun. 12 , 6425 (2021) ¹⁷
Plasmonic	~10	1.4×10^{-7}	725–800	2×10^{-9}	1.8×10^{-8}	ACS Photonics 10 , 1529 (2023) ¹⁸
BIC	~4000	0.5–2	1200	4×10^{-5}	4×10^{-3}	Nano Lett. 20 , 8745 (2020) ²³
BIC	~188	~0.07	1570	1.18×10^{-5}	1.6×10^{-4}	Science 367 , 288 (2020) ²⁴
PhC	~100	~100	742	2.8×10^{-3}	6.7×10^{-4}	Adv. Funct. Mater. 33 , 2308484 (2023) ¹⁹
PhC	~100	~100	843	1×10^{-3}	4.7×10^{-4}	Adv. Opt. Mater. 13 , 2402686 (2023) ²⁰
PhC	8000	~1.18	1510	5.21×10^{-9}	N/A	Nanophotonics 13 , 4029 (2024) ²¹
PhC	5600	~0.3	1500	3×10^{-11}	4.4×10^{-9}	Nano Lett. 24 , 11327 (2024) ²²
Anapole	~10	~7	1440	1.18×10^{-8}	6.1×10^{-10}	Adv. Mater. 37 , 2418257 (2024) ³¹
Anapole	~5	~1.17	~800	1.9×10^{-5}	1.9×10^{-5}	Nano Lett. 18 , 3695 (2018) ²⁹
Mie	~20	~0.15	1400	3.4×10^{-10}	1.87×10^{-12}	Nat. Commun. 12 , 5597 (2021) ²⁵
Mie	~10	~1.58	900	5×10^{-8}	3.77×10^{-9}	Laser Photonics Rev. 16 , 2100604 (2022) ²⁶
Mie	~10	~10	820	2×10^{-6}	9.75×10^{-7}	Laser Photonics Rev. 15 , 2000521 (2021) ²⁷
Metasurface	~75	~1.38	940	2×10^{-4}	8.3×10^{-5}	Nano Lett. 22 , 9652 (2022) ⁴⁰
GMR	~4000	~110	1550	3×10^{-8}	2.03×10^{-5}	Phys. Rev. Lett. 127 , 153901 (2021) ²⁸
CBG/EBG	~260	~1.12	1310	2.32×10^{-5}	1.21×10^{-2}	Nano Lett. 24 , 11676 (2024) ⁴²

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