

## Supplementary Materials for

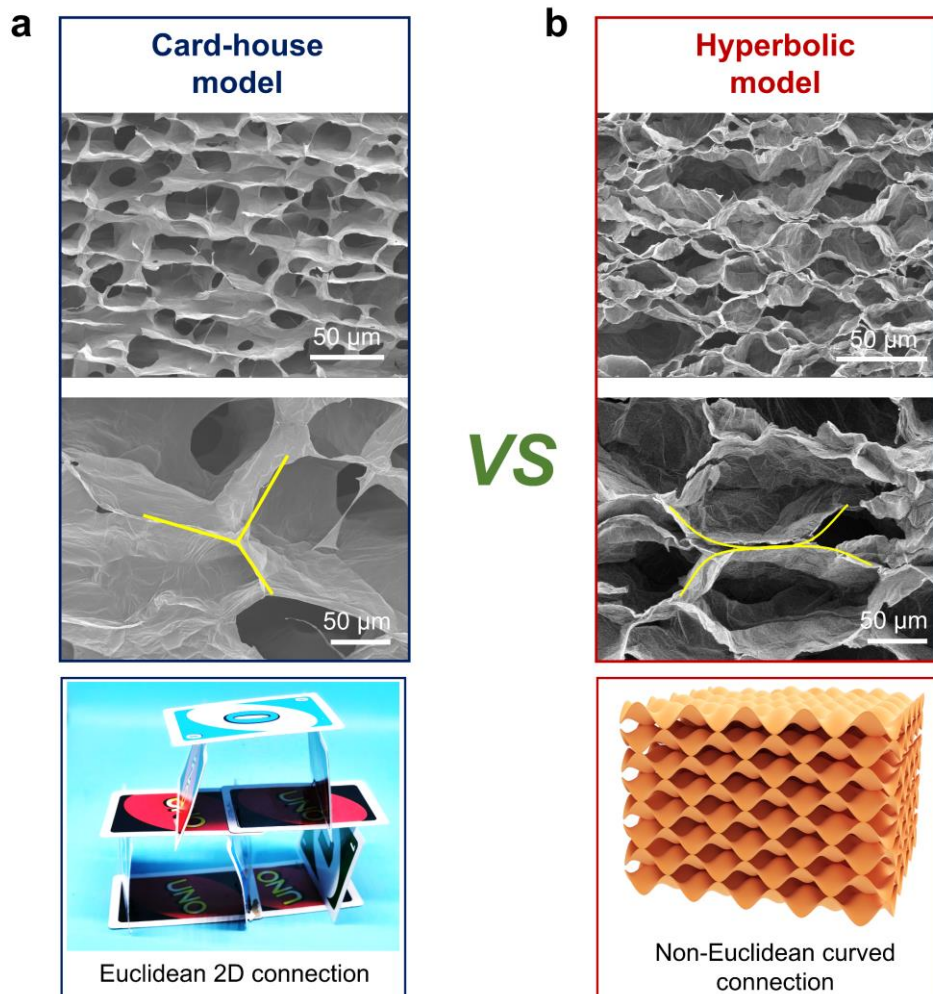
### **Hyperbolic graphene framework with optimum efficiency for conductive composites**

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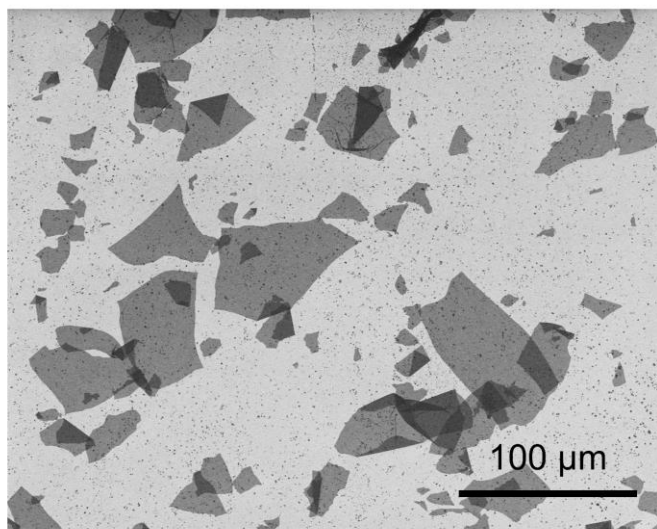
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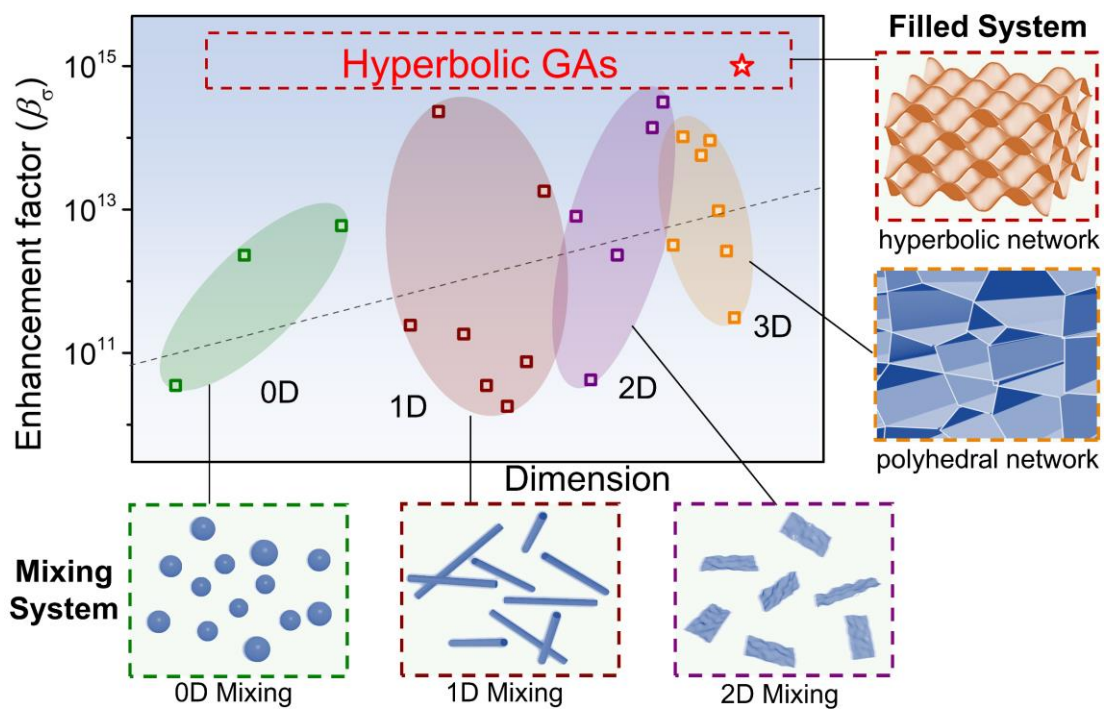
## Supporting figures



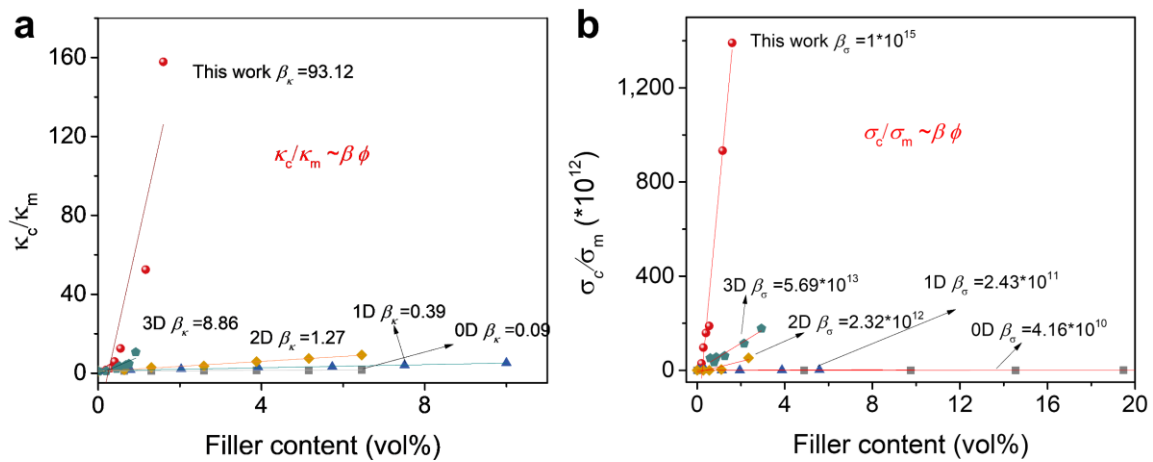
**Figure S1.** Polyhedral “card-house” model (by conventional methods) and hyperbolic model (by hydroplastic foaming) of 3D graphene framework. Photo Credit: Kai Pang, Zhejiang University.



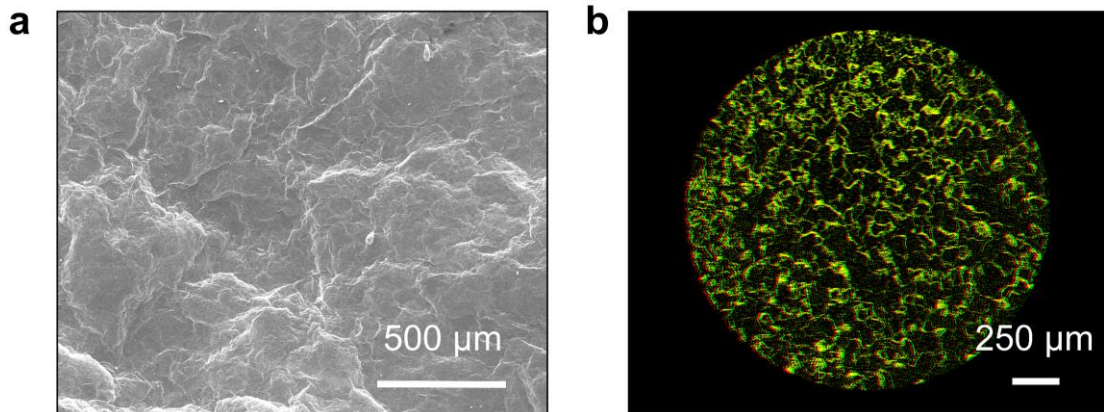
**Figure S2.** SEM image of GO sheets.



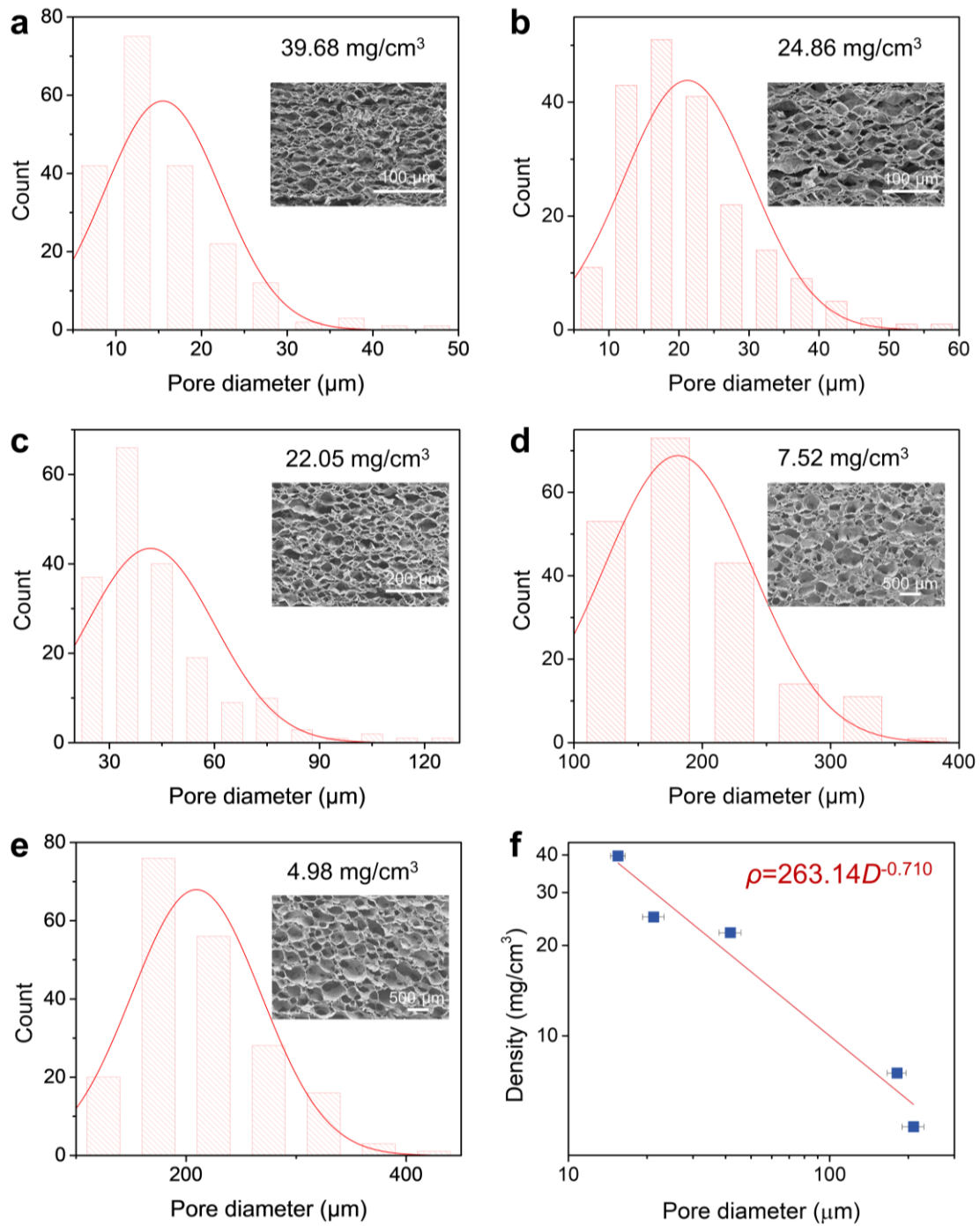
**Figure S3.** Electrical enhancement factor of composites with different nanofillers<sup>1-21</sup>.



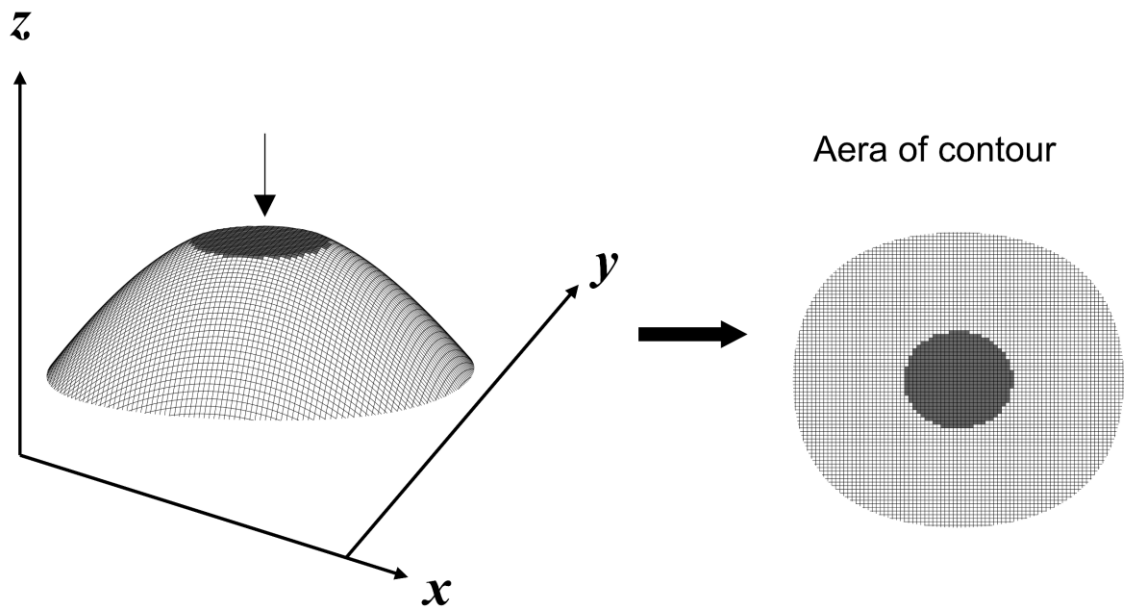
**Figure S4.** Comparison of typical enhancement factors of 0D, 1D, 2D and 3D nanofillers<sup>1-3,16,22,23</sup>.



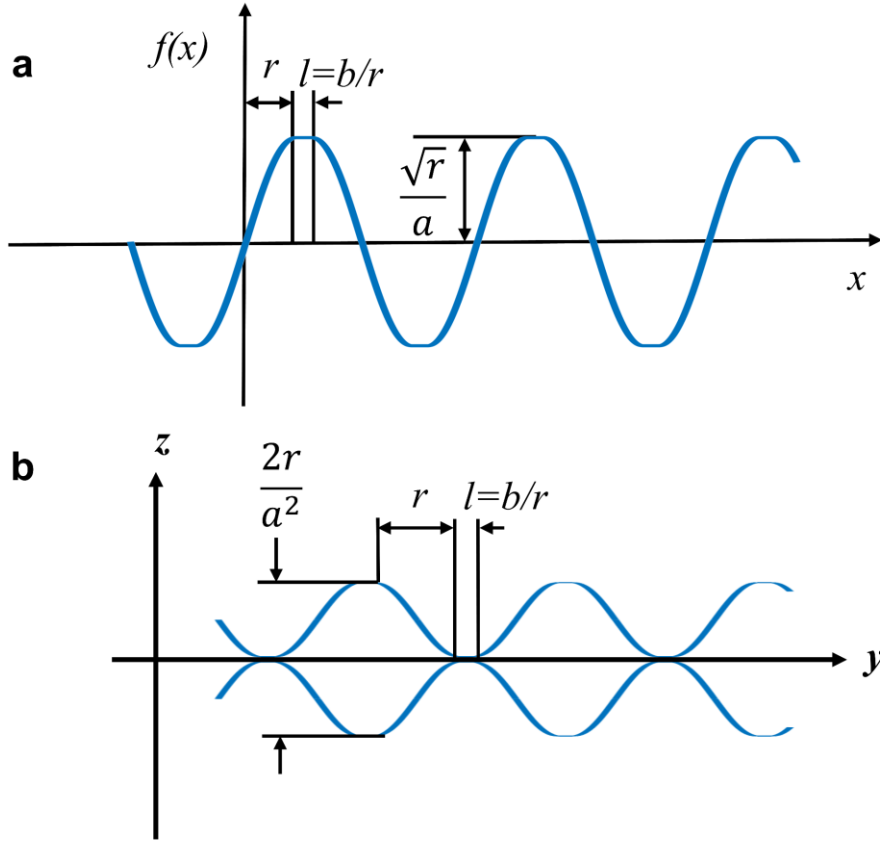
**Figure S5. (a) SEM and (b) CT images of the surface of HGA.**



**Figure S6.** (a-e) Pore size distributions of HGAs with different densities. (f) Densities of HGAs as a function of pore sizes.



**Figure S7.** Side and top view of the contact area between curved graphene sheets.



**Figure S8.** Model calculation of contact area of hyperbolic graphene networks.

Based on previous report, the modified model is proposed as followed in Figure S8A:

$$f(x) = \begin{cases} -\frac{\sqrt{r}}{a}, & x \in [-\frac{k}{2}(r+l), -\frac{kr}{2}) \\ \frac{\sqrt{r}}{a} \sin\left(\frac{\pi x}{r}\right), & x \in [-\frac{kr}{2}, \frac{kr}{2}) \\ \frac{\sqrt{r}}{a}, & x \in [\frac{kr}{2}, \frac{k}{2}(r+2l)) \\ \frac{\sqrt{r}}{a} \sin\left[\frac{\pi(x-l)}{r}\right], & x \in [\frac{k}{2}(r+2l), \frac{k}{2}(3r+2l)) \\ -\frac{\sqrt{r}}{a}, & x \in [\frac{k}{2}(3r+2l), \frac{3k}{2}(r+l)) \end{cases}$$

$$f(y) = \begin{cases} -\frac{\sqrt{r}}{a}, y \in [-\frac{k}{2}(r+l), -\frac{kr}{2}) \\ \frac{\sqrt{r}}{a} \sin\left(\frac{\pi y}{r}\right), y \in [-\frac{kr}{2}, \frac{kr}{2}) \\ \frac{\sqrt{r}}{a}, y \in [\frac{kr}{2}, \frac{k}{2}(r+2l)) \\ \frac{\sqrt{r}}{a} \sin\left[\frac{\pi(y-l)}{r}\right], y \in [\frac{k}{2}(r+2l), \frac{k}{2}(3r+2l)) \\ -\frac{\sqrt{r}}{a}, y \in [\frac{k}{2}(3r+2l), \frac{3k}{2}(r+l)) \end{cases}$$

where a and b are the coefficients related to the HGA geometry,  $k \in \mathbb{Z}$  (arbitrary integer).

As shown in Figure S8B, because hyperbolic curvature follows Gaussian curvature characteristics, so

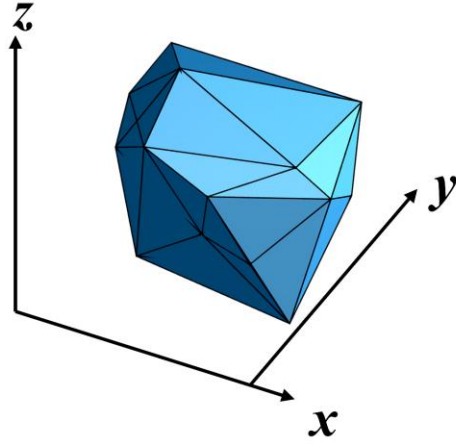
$$z(x, y) = f(x) * f(y)$$

The contact area of a cell in parallel direction:  $S_c = l^2$ , ( $l = b/r$ )

The surface area of a cell:  $S = \iint \sqrt{1 + \left(\frac{dz}{dx}\right)^2 + \left(\frac{dz}{dy}\right)^2} dx dy$

The volume of a cell:  $V = \left(\frac{2\sqrt{r}}{a}\right)^2 * (2r + 2l) * (2r + 2l)$

The density of HGA:  $\rho = S * t * 2.26 / V$ , t is the thickness of the pore wall.



**Figure S9.** Theoretical calculation of contact area of polyhedral graphene networks.

In order to describe the random structure of GAs, taking randomly distributed points in the unit space as the body center, we learn from the generation principle of Tyson polyhedrons to generate a convex polyhedron with random structures as shown in Figure S9.

The length of the three sides of each plane:

$$a_i = B_i C_i = \sqrt{(x_{2i} - x_{3i})^2 + (y_{2i} - y_{3i})^2 + (z_{2i} - z_{3i})^2}$$

$$b_i = A_i C_i = \sqrt{(x_{1i} - x_{3i})^2 + (y_{1i} - y_{3i})^2 + (z_{1i} - z_{3i})^2}$$

$$c_i = A_i B_i = \sqrt{(x_{1i} - x_{2i})^2 + (y_{1i} - y_{2i})^2 + (z_{1i} - z_{2i})^2}$$

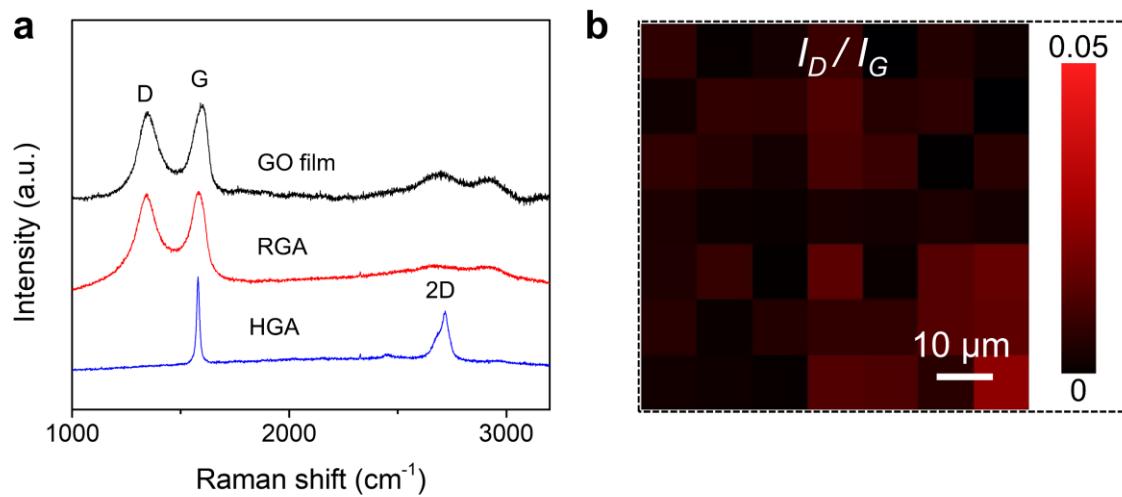
$$S_i = t * \Sigma p_i, \quad p_i = a_i + b_i + c_i$$

$$S = \Sigma S_i, \quad S_i = \frac{\sqrt{p_i * (p_i - a_i) * (p_i - b_i) * (p_i - c_i)}}{4}$$

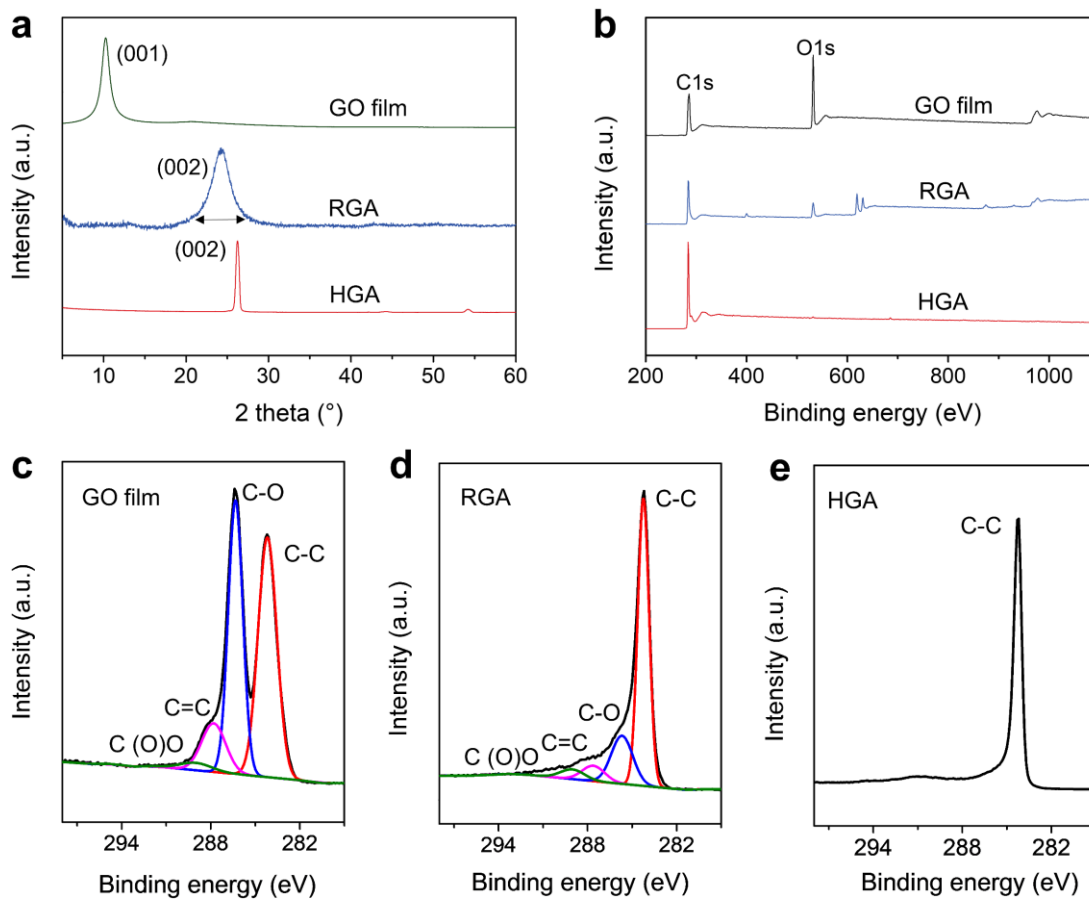
$$\rho = S * t * 2.26 / V$$

The volume V of the resulting polyhedron is dependent on the randomly distributed points in the unit space.

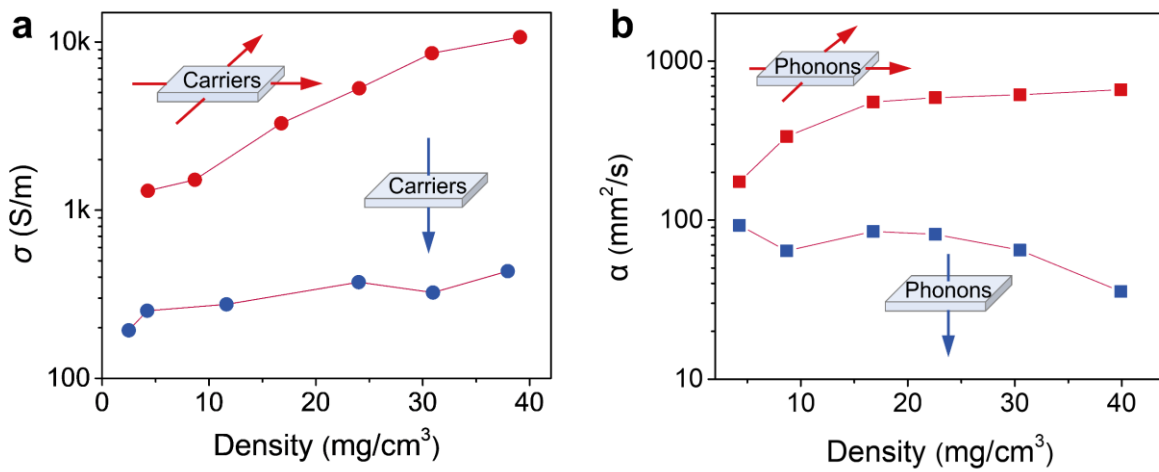
According to the above formula, the contact area between graphene sheets is obtained as shown in Fig. 2H.



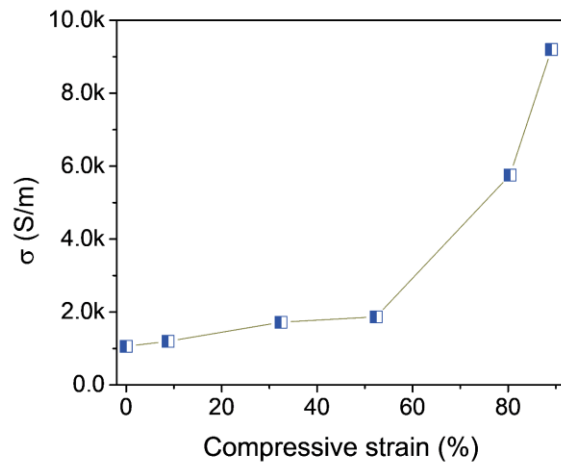
**Figure S10. Raman characterization.** (a) Raman spectra of GO film, RGA and HGA. (b) Raman mapping of HGA.



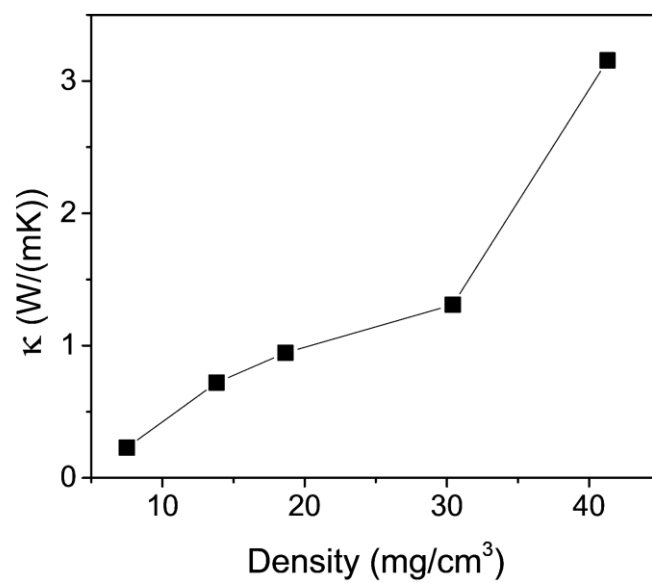
**Figure S11.** (a) XRD patterns and (b-e) XPS spectrum of GO film, RGA and HGA.



**Figure S12.** (a) The in-plane and through-plane electrical conductivity and (b) thermal diffusion coefficient of HGAs.



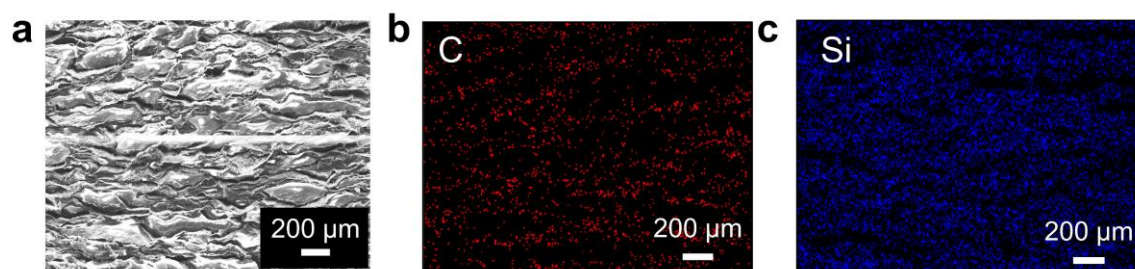
**Figure S13.** Electrical conductivity of HGA with different compressive strains.



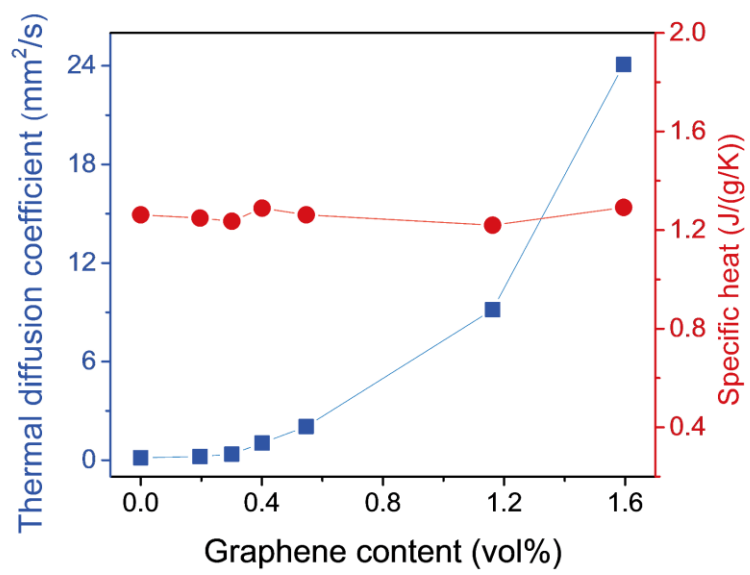
**Figure S14.** Thermal conductivity of freeze-dried GAs with different densities.



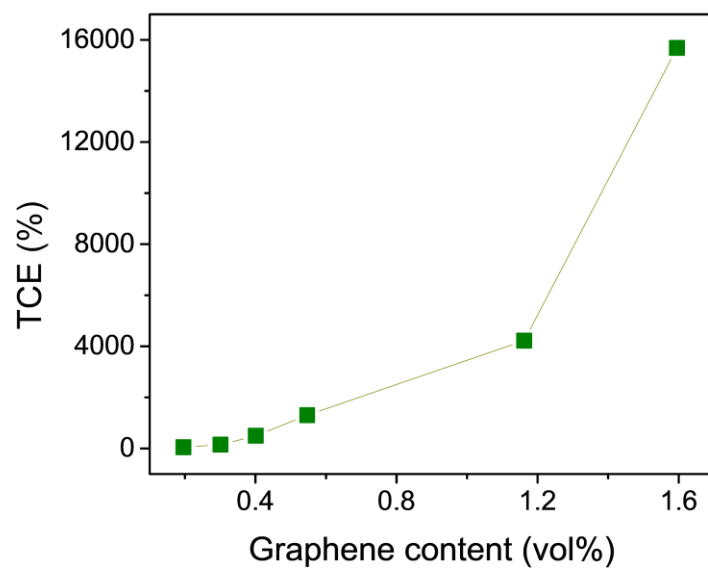
**Figure S15.** The digital photo of PGC after vacuum infusion. Photo Credit: Kai Pang, Zhejiang University.



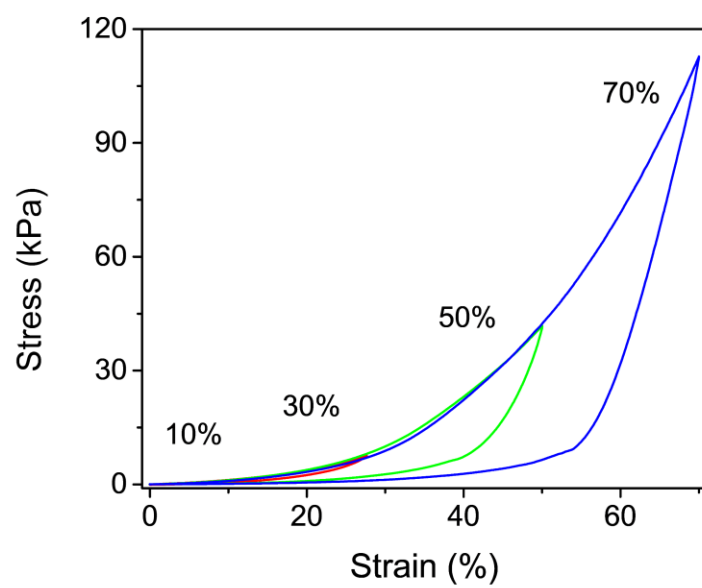
**Figure S16. Elemental mappings of PGC.** (a) SEM mapping image. Elemental (b) C and (c) Si mapping images.



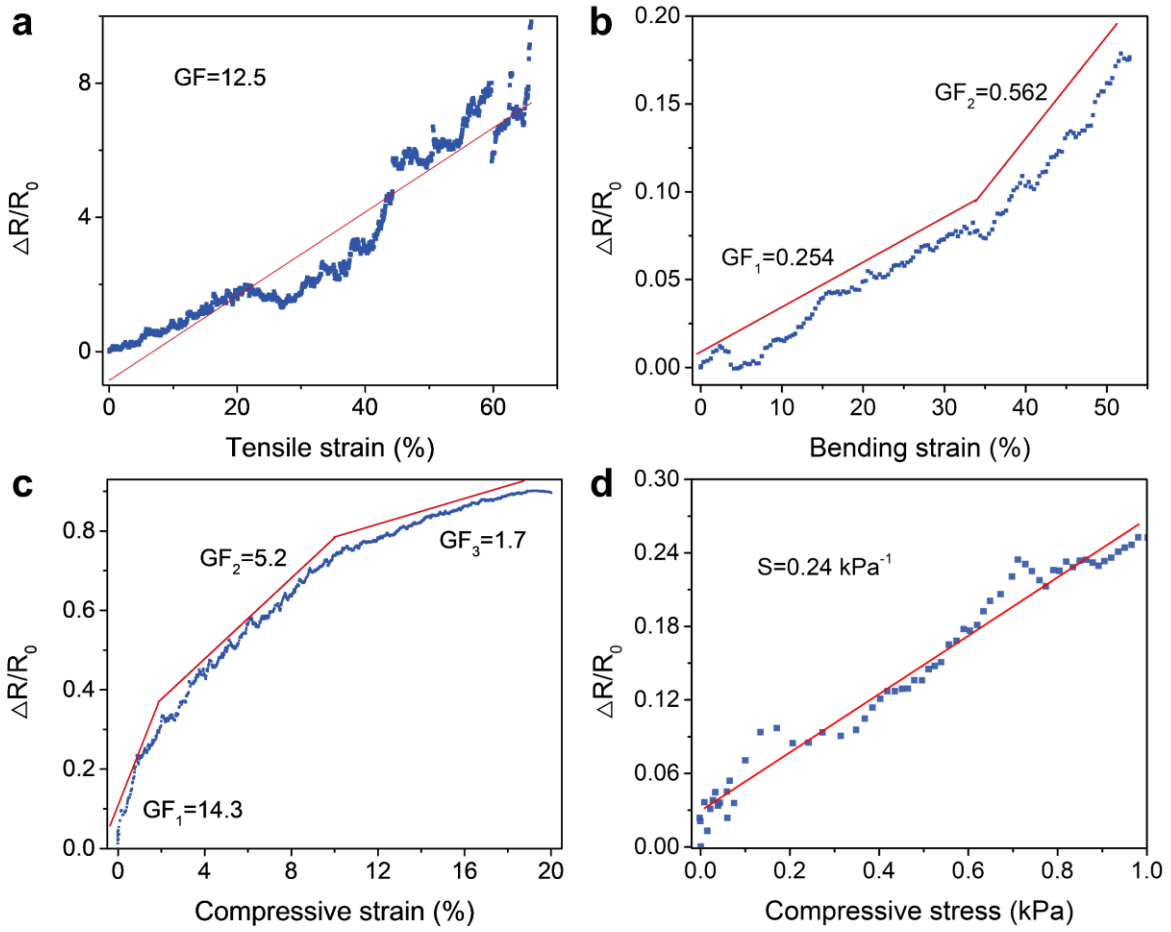
**Figure S17.** Thermal diffusion coefficient and specific heat of PGCs with different graphene loadings.



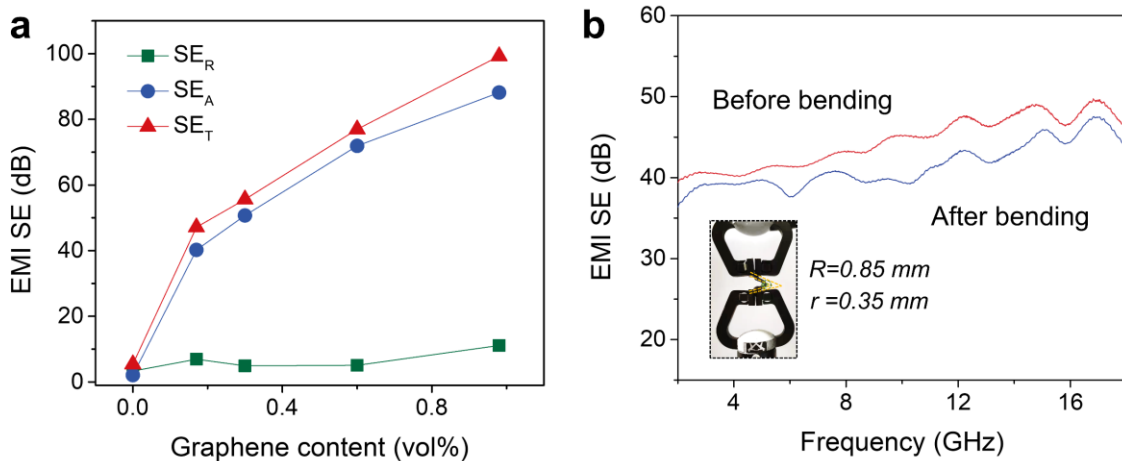
**Figure S18.** TCE of PGCs with different graphene loadings.



**Figure S19.** The compressive curves of PGC at various strains.



**Figure S20.** The  $\Delta R/R_0$  changes of PGC with (a) tensile strain, (b) bending strain, (c) compressive strain and (d) compressive stress.



**Figure S21. EMI SE and mechanical stability of PGC.** (a) Average  $SE_T$ ,  $SE_R$ , and  $SE_A$  of the PGCs with various graphene loadings. (b) EMI SE values of PGC before and after bending 1000 cycles. Photo Credit: Kai Pang, Zhejiang University.

## **Supporting movies**

### **Movie S1.**

Heat diffusion of PDMS and PGC for a high-power LED lamp. Play speed is 10x of the actual speed.

### **Movie S2.**

Heat transfer of PDMS and PGC for a high-power LED lamp. Play speed is 10x of the actual speed.

## Supporting references

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