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**Sensitivity Analysis of Mixing Front Control between Saline and Fresh Groundwater in
the Marvdasht-Kharameh Aquifer Using the MODPATH-MODFLOW Model**

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12 **Abstract**

13 This study analyzes the sensitivity of groundwater flow and the mixing fronts of saline and fresh transient
14 groundwater in the Marvdasht-Kherameh aquifer using the MODPATH-MODFLOW model. In groundwater flow
15 modeling, IPCC scenarios (such as RCPs and SSPs) are used to predict climate changes, including variations in
16 temperature and precipitation, which can directly impact groundwater levels, aquifer recharge, and groundwater
17 flow patterns. Uncertainty analysis was conducted using the First-Order Reliability Method (FORM) to assess the
18 aquifer's sensitivity to groundwater level changes. The findings indicate that the flood volume entering water bodies
19 diminishes during wet and dry periods as it mixes with saline water. The critical scenario involves water infiltration
20 into the aquifer, highlighted by FORM results, showing a homogeneous flow pattern in the affected region.
21 Excessive groundwater extraction has led to significant flow disruption risks in concentrated healthy areas. Saline
22 water infiltration from the wetland and lake accelerates desiccation. It maintains stable flow in the southeastern
23 plain, leading to salt accumulation and destruction of the aquifer's recharge structure in central regions. Effective
24 management strategies are necessary to preserve the region's ecological and hydrological balance. This research
25 provides valuable insights into the interactions between saline and fresh groundwater and their impact on aquifer
26 stability and wetland health.

27

28 **Keywords:** Sensitivity Analysis, MODPATH-MODFLOW Model, Saline and Fresh Groundwater Interface,
29 Marvdasht-Kherameh Aquifer

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32 **1. Introduction**

33 Increasing challenges such as climate change, excessive groundwater extraction, and pollutant intrusion profoundly
34 impact the delicate balance between saline and fresh groundwater fronts. These environmental and human-induced
35 changes often lead to the displacement and mixing of these fronts, jeopardizing groundwater resources' quality and
36 availability (Roy & Datta, 2020; Sharma et al., 2021). Given the complexity of these dynamics, traditional
37 groundwater management approaches often fail to provide accurate and effective solutions (Amanambu et al., 2020).
38 The mixing front refers to the interface where saline and fresh groundwater meet and interact within an aquifer. This
39 front plays a crucial role in determining groundwater quality, especially in areas where salinity intrusion is a
40 concern. The movement and extension of the mixing front are influenced by several factors, including aquifer
41 recharge, extraction rates, and external saline sources. In this study, we focus on how the mixing front behaves and
42 extends, particularly under varying climatic and extraction scenarios in the Marvdasht-Kherameh aquifer.
43 This is where sensitivity analysis becomes indispensable. By identifying critical parameters and quantifying their
44 impact on the system's behavior, sensitivity analysis helps better understand the hydrodynamic processes governing
45 groundwater flow (Ghadeer & Maghrebi, 2023; Vatanchi & Maghrebi, 2022). Moreover, it enables more precise
46 predictions of how various factors, such as changes in climate or extraction rates, affect groundwater quality and
47 availability (Cao et al., 2020; Moutsopoulos, 2021). Therefore, sensitivity analysis not only enhances modeling
48 accuracy but also informs decision-making, such as the optimal placement of wells, artificial recharge systems, and
49 the evaluation of development projects (Pargar et al., 2024; Tareghian et al., 2024). Through these applications,
50 sensitivity analysis offers a path to more efficient and sustainable management of groundwater resources,
51 particularly in regions facing severe water scarcity (Mohammadi et al., 2021; Ma et al., 2024; Boni et al., 2020).
52 Zhang et al. (2010) evaluated pollutant concentration levels in an airport area using the probabilistic reliability
53 assessment method (PRAM). Sensitivity analysis helps quantify and assess different factors' contribution to the
54 overall uncertainty in model predictions. Still, uncertainty can arise from various sources, including measurement
55 errors, parameter estimation, model structure, and external factors.
56 Iqbal et al. (2018) investigated the effects of groundwater pumping and river bank filtering (RBF) on the installation
57 of wells, pumping rates in flow paths, travel time, pumping size, determining coverage area, and mixing of
58 groundwater in a pumping well in the Penang region, Malaysia. The results indicated that river water movement to
59 the aquifer is generally slow, depending on pumping rates and the well's distance from the river. Alimonti et al.

60 (2017) conducted an uncertainty analysis using a reliability assessment to quantify soil variability. Using the First-
61 Order Reliability Method (FORM), the reliability index and failure probability demonstrated a practical and
62 straightforward method for simultaneous implementation. Their work analyzed the potential effects of aquifer
63 compaction in the Scarlino plain of Italy resulting from the expansion of hydraulic barriers for water reclamation.
64 Dey and Prakash (2022) stated that coastal areas are densely populated due to social and economic benefits,
65 increasing the demand for fresh water. Coastal aquifers acting as large freshwater reservoirs can meet this growing
66 demand. Performance evaluation results indicate the method's application for managing saltwater intrusion while
67 maximizing freshwater pumping in coastal aquifers. Feo et al. (2018) mentioned that the MODFLOW model is
68 currently the most popular tool for studying groundwater flow and aquifer modeling. To simplify the MODFLOW
69 interface, Graphical User Interfaces (GUIs) are used to create model definition files and visualize and interpret
70 results (Baradaran and Ameri 2023; Ayar et al. 2022). They developed the FloPy interface for MODFLOW,
71 allowing users to import and utilize simulation data generated using Python.

72 Considering these challenges, this study investigates how sensitivity analysis can be applied to groundwater
73 modeling, specifically addressing key scientific questions such as the role of aquifer diffusion coefficients in long-
74 term groundwater flow predictions and the effects of recharge projects on salinity levels. The study aims to advance
75 the understanding of how these factors interact and contribute to groundwater management strategies (Doherty
76 2001; Feo et al. 2018). The primary innovation of this research lies in the integration of advanced probabilistic
77 methods (Alimonti et al. 2017; Dey and Prakash 2022), such as FORM uncertainty analysis, with GIS-based spatial
78 modeling to evaluate the dynamic behavior of aquifer diffusion coefficients over extended periods. While methods
79 for creating continuous raster maps exist, this study introduces a novel approach by combining these techniques with
80 the MODFLOW and MODPATH models to enhance the accuracy of long-term predictions and optimize
81 groundwater resource management strategies, particularly in regions vulnerable to salinity intrusion.

82

83 **2. Materials and Methods**

84 **2.1. Study Area Introduction**

85 The Marvdasht-Kharameh study area is in Fars Province, Iran, covering 3926.1 km², including 1823.4 km² of
86 highlands and 2102.7 km² of plains (Raja et al. 2019). This area consists of six plains: Dashtak-Doroodzan, Mayin-
87 Bidkal, Ramjerd, Dashtbal-Laneh Tavous, Marvdasht-Karbal, and Kharameh. The Marvdasht-Kharameh study area

88 contains an alluvial aquifer with a total area of 1470.5 km², playing a crucial role in the groundwater supply for the
89 region (Ahmadi Akhormeh et al. 2015). This aquifer is divided into two main sections: the Marvdasht aquifer
90 (1221.5 km²) and the Kharameh aquifer (249 km²). To measure the depth and level of groundwater in this area,
91 water level measurements have been conducted in 72 observation wells (Ahmadi Akhormeh et al. 2015; Baradaran
92 et al. 2024). These measurements began in the 1991-1992 water year for the Kharameh Plain, 2000-2001 for the
93 Marvdasht-Karbal Plain, and 2003-2004 for the other plains. Figure 1 shows the geography of the study area and
94 illustrates the location of the observation wells drilled in the Marvdasht-Kharameh aquifer area by the black point on
95 the aquifer surface.

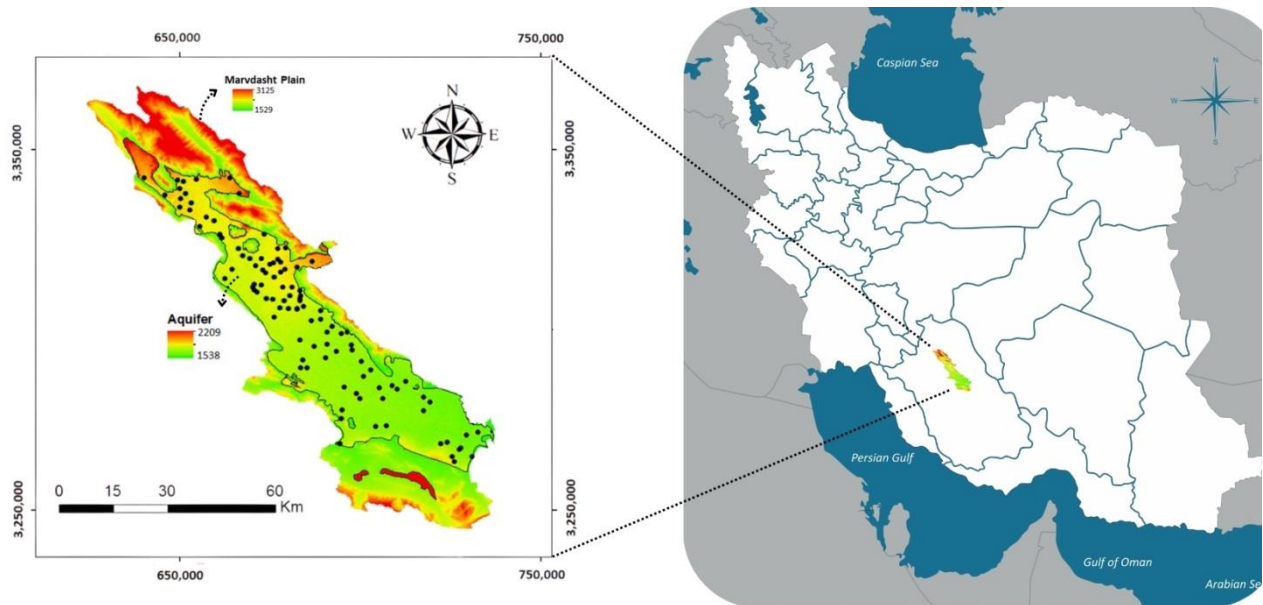


Figure 1. The geographical location of the Marvdasht-Kharameh study area with
the location of observation wells (black points)

96
97 **2.2. Numerical Modeling**

98 The Groundwater Modeling System (GMS) software is one of the most advanced tools for groundwater modeling,
99 developed by Aquaveo (Samani 2024). This software offers extensive capabilities, including modeling groundwater
100 flow using models like MODFLOW, pollutant transport analysis with models such as MT3DMS and RT3D, and
101 particle tracking with the MODPATH model (Mohammed et al. 2023). GMS allows for importing and processing
102 geological, hydrological, and hydrogeological data and utilizes advanced graphical tools for data visualization and
103 results interpretation. The software can create complex three-dimensional models and conduct sensitivity analyses

104 and calibrations. Additionally, GMS has powerful capabilities for simulating the impacts of human activities, such
105 as agriculture, industry, and urbanization, on groundwater resources and provides management solutions to preserve
106 and improve water quality (Amiri et al. 2023; Yazdi et al. 2024).

107 One of the essential and widely used models in GMS is the MODPATH model, which tracks particle paths in
108 groundwater environments (Alaviani et al. 2018). MODPATH is a particle-tracking model that operates based on the
109 results of flow models like MODFLOW. This model uses hydrodynamic data and boundary conditions to simulate
110 the movement paths of particles in groundwater environments. In MODPATH, hypothetical particles are placed at
111 various points in the model, and their paths are tracked based on water flow. This method allows researchers to
112 predict groundwater pollutants' paths and travel times (Alaviani et al. 2018). The capabilities of the MODPATH
113 model include simulating particle paths in complex flow systems, analyzing forward and backward tracking paths,
114 and evaluating particle travel times. This model can help identify areas vulnerable to pollution, determine its
115 sources, and spread assessments. MODPATH is also helpful in groundwater resource management analyses, as it
116 can evaluate the effects of water extraction, water injection, and other management activities on groundwater
117 distribution and movement (Ghandehari et al. 2024).

118 The combination of GMS's advanced capabilities and various models, including MODPATH, makes this software a
119 robust and comprehensive tool for analyzing and managing groundwater resources. GMS and its diverse models
120 help researchers and water resources managers analyze and manage complex groundwater issues with high accuracy
121 and efficiency. In particular, the ability of the MODPATH model to accurately track particle paths and predict
122 pollutant spread provides a critical tool for protecting groundwater quality and developing effective management
123 strategies (Amiri et al. 2023; Alaviani et al. 2018; Ghandehari et al. 2024). This study used the MODPATH-
124 MODFLOW model to analyze the sensitivity of controlling the mixing cycles of saline and fresh groundwater fronts
125 in the Marvdasht-Kharameh aquifer. The input parameters for the model are presented in Table 1.

126 To accurately simulate the mixing front between saline and fresh groundwater, the boundaries of the mixing front
127 were defined using salinity gradients within the aquifer. The movement and extension of the mixing front were
128 tracked through the MODFLOW and MODPATH models, which were employed to simulate groundwater flow and
129 particle transport respectively. These models incorporate several key parameters, including hydraulic conductivity,
130 recharge rates, and groundwater extraction rates. The boundaries of the mixing front were dynamically simulated by
131 evaluating salinity concentrations across the aquifer grid at various time intervals. The model results show that the

132 mixing front shifts in response to seasonal variations in recharge and changes in extraction rates. This dynamic
 133 behavior was captured by the combination of MODFLOW's flow modeling and MODPATH's particle tracking
 134 capabilities, which allowed us to simulate the movement and dispersion of the saline and fresh groundwater
 135 interface.

136 **Table 1.** Primary and secondary parameters used in numerical modeling

Data Type	Primary Model Parameters	Secondary Model Parameters	Source
Topography	Digital elevation maps of the region	Slope maps and directions	(Akter and Ahmed 2021)
	Topology maps of the region	Finite difference grid of surface features	
Remote Sensing	MODIS satellite images	Vegetation cover maps and other data	(Mokarram et al. 2022)
Soil	Soil permeability data (K)	Estimation of hydraulic conductivity in the plain	(Ahani and Noshadi 2019)
	Geological maps of the study area	Drawing and refining transmissivity contour lines	
	Aquifer bedrock layer	Interpolated contour lines on the finite difference grid of the aquifer bedrock	
Geology	Well logs	-	(Mokarram et al. 2022)
	Geophysical data from consultants	-	
	Aquifer basin boundary spatial layer and saturated aquifer boundary	Precise determination of boundary conditions	
Land Use	Land use maps	Detailed land status and changes over time	(Heydari and Jabbari 2022)
	Rainfall data	Isohyet maps	
Meteorology	Evapotranspiration data	Iso-evapotranspiration maps	(Ahani and Noshadi 2019)
	Surface runoff input and output data within the plain	Refinement of transmissivity values, water levels, and river network bed	(Heydari and Jabbari 2022)
	Observation well data	Flow path determination using the Kriging method	(Mokarram et al. 2022)
Hydrogeology	Extraction well data	-	(Ahani and Noshadi 2019)
	Input and output flows at reservoir sites or recharge basins	Precise determination of boundary conditions	
	Aquifer storage coefficient	SS	
	Specific yield estimation of unconfined aquifer	SY	
Water Quality	EC data from wells	Refining areas with salinity issues and problem-free zones	(Raja and Parsinejad 2023)
Human Activities	Construction points for dams and canals	-	(Ahani and Noshadi 2019)

137

138 It is important to understand the distinction between primary and secondary model parameters, as this distinction
 139 plays a crucial role in how the model is built and how accurately it simulates the system.

140 Primary parameters are the core physical characteristics of the system that directly influence the modeled processes.

141 They form the foundation of the model and are essential for constructing the simulation. Primary parameters include

142 factors such as soil permeability, aquifer properties, and elevation maps. These parameters directly affect the main
143 dynamics being studied, such as the movement of water or materials, and are integral to the functioning of the
144 model. Without accurate primary data, the model's ability to represent the system accurately would be compromised.
145 In contrast, secondary parameters are derived from the primary data and help to enhance the model's accuracy or
146 simulate specific phenomena that are not directly tied to the core processes. These parameters provide additional
147 context and detail to the simulation. For example, land use maps, rainfall data, and water quality data are considered
148 secondary parameters. While they are essential for improving the model's precision and understanding the broader
149 environmental influences, they do not directly drive the core processes of the system being modeled. Essentially,
150 secondary parameters enrich the model, providing a more complete picture, but they are not critical to its
151 fundamental structure.

152 By distinguishing between these two types of parameters, the model can more effectively simulate the real-world
153 system, ensuring that primary factors govern the key dynamics while secondary factors provide additional context
154 for accuracy and specificity.

155 **2.3. Kriging Interpolation**

156 Spatial zonation was performed using the Kriging interpolation method in GIS software. First, the particle travel
157 distances for each coordinate were determined. These data were then used as input for the Kriging model. Kriging is
158 an advanced interpolation technique that estimates values at unknown points based on measured values at known
159 points, considering spatial correlations and the variogram structure. Due to its ability to model spatial variations,
160 Kriging was an ideal choice for zonation and detailed particle distribution analysis in complex environments.
161 Kriging enabled a more accurate simulation of spatial particle dispersion and creating spatial zonation maps,
162 significantly contributing to subsequent analyses and management decisions. In Kriging interpolation, the prediction
163 of the unknown value at a location x_0 is given by a weighted sum of the known values (Eq. 1).

$$\hat{Z}(x_0) = \sum_{i=1}^n \lambda_i Z(x_i) \quad (1)$$

164
165 where $\hat{Z}(x_0)$ is the predicted value at x_0 , $Z(x_i)$ is the known value at x_i , λ_i is the weight associated with the known
166 value at x_i , and n is the number of known data points. The weights λ_i are determined by minimizing the estimation
167 variance subject to the constraint that the estimator is unbiased. This leads to the system of linear equations (Eq. 2):

$$\sum_{j=1}^n \lambda_j \gamma(x_i, x_j) + \mu = \gamma(x_i, x_0) \quad , \quad i = 1, 2, \dots, n \quad (2)$$

168

169 where $\gamma(x_i, x_j)$ is the semivariance between the points x_i and x_j , and μ is a Lagrange multiplier used to enforce the
 170 unbiasedness constraint.

171 **2.4. R-squared**

172 R^2 measures the proportion of the variance in the dependent variable that is predictable from the independent
 173 variables in a regression model. It is also known as the coefficient of determination and is widely used to evaluate
 174 the goodness of fit in regression analysis (Eq. 3).

$$R^2 = 1 - \frac{SS_{res}}{SS_{tot}} \quad , \quad SS_{res} = \sum_{i=1}^n (y_i - \hat{y}_i)^2 \quad , \quad SS_{tot} = \sum_{i=1}^n (y_i - \bar{y})^2 \quad (3)$$

175

176 where SS_{res} (Residual Sum of Squares) is the sum of the squared differences between the observed values and the
 177 predicted values from the model, and SS_{tot} (Total Sum of Squares) is the sum of the squared differences between the
 178 observed values and the mean of the observed values. It should be noted that y_i is the observed value and \hat{y}_i is the
 179 predicted value from the regression model, and \bar{y} is the mean of the observed values.

180 **2.5. FORM (First-Order Reliability Method)**

181 The First-Order Reliability Method (FORM) is a foundational technique in structural and engineering reliability
 182 analysis used to evaluate the probability that a system will fail under given uncertainties (Liu et al. 2023). The
 183 method transforms the input variables, often uncertain or random, into a standard normal space, making the complex
 184 problem more manageable. This design point is found through an optimization process, where the method linearizes
 185 the limit state function at this critical location (Hu et al. 2023). FORM is precious in scenarios where direct
 186 simulation methods, like Monte Carlo simulations, would be too computationally expensive. Due to its balance
 187 between computational efficiency and accuracy, it is extensively used in various engineering fields, including civil,
 188 mechanical, and aerospace engineering. However, its reliability can decrease for problems involving highly
 189 nonlinear behaviors or multiple failure modes, where more sophisticated or higher-order methods might be
 190 necessary. Despite its limitations, FORM remains a cornerstone in reliability analysis for engineering design and
 191 risk assessment. The key formula (Eq. 4) for the FORM is the expression for the probability of failure P_f , which is
 192 based on the reliability index β :

$$P_f = \Phi(-\beta) \quad (4)$$

193

194 where Φ is the cumulative distribution function (CDF) of the standard normal distribution, and β is the reliability
195 index, representing the distance from the origin to the limit state surface in standard normal space.

196 **3. Model Calibration and Validation**

197 In this study, the Marvdasht-Kharameh aquifer model was developed to simulate groundwater flow and assess the
198 sensitivity of saline and fresh groundwater fronts. The model was created using the Groundwater Modeling System
199 (GMS) software, which offers advanced capabilities for groundwater modeling, including MODFLOW for flow
200 simulation and MODPATH for particle tracking. After the model design and data input, calibration and validation
201 were performed to ensure accuracy in predicting future aquifer behavior under various conditions.

202 The data input for the model was sourced from multiple datasets. Topographic data were represented by digital
203 elevation maps (DEM), which were used to simulate surface features and define the spatial distribution of the
204 groundwater system. Soil permeability and geological maps of the study area were used to characterize the
205 hydrogeological properties of the aquifer. Observational data for groundwater levels, precipitation, and
206 evapotranspiration were gathered over 127 months to model seasonal and long-term variations. Furthermore,
207 MODFLOW and MODPATH models were employed to simulate groundwater flow and the movement of particles
208 in the aquifer. Boundary conditions were defined using regional hydrogeological data to represent the aquifer
209 boundaries and recharge zones.

210 The model calibration was conducted over 127 months. The primary objective was to adjust parameters such as
211 hydraulic conductivity (K) and other hydrogeological factors to match the model's outputs with observed data. This
212 process involved iterative adjustments to minimize discrepancies between simulated and observed groundwater
213 levels. Parameters were calibrated for each aquifer layer, ensuring accurate groundwater flow simulations. The
214 calibration process was continually refined by incorporating updated observational data. Figure 2 compares
215 observed and simulated head values, confirming the model's calibration accuracy.

216 For model validation, observational data from the last 31 months of the 127-month study period were used,
217 providing an independent dataset for testing the model's predictive accuracy. The model successfully simulated the
218 future behavior of the aquifer, showing good agreement with observed data. The comparison between simulated and

219 observed groundwater levels demonstrated that the model could replicate real-world conditions effectively. In
 220 addition, the R² values presented in Table 2 reflect the high accuracy of the model in simulating aquifer behavior.

221 **Table 2.** R-squared reduction in the validation stage of the Marvdasht-Kharameh plain model

Property	Value
Mean Residual (Head)	-0.92 (m)
Mean Absolute Residual (Head)	1.86 (m)
Root Mean Squared Residual (Head)	0.92 (m)
Mean Residual (Flow)	0 (m ³ /s)
Absolute Residual (Flow)	0 (m ³ /s)
Root Mean Squared Residual (Flow)	0 (m ³ /s)
Mean Weighted Residual (Head+Flow)	0 (m ³ /s)
Mean Absolute Weighted Residual (Head+Flow)	0 (m ³ /s)
Root Mean Squared Weighted Residual (Head+Flow)	0 (m ³ /s)
Sum of Squared Weighted Residual (Head+Flow)	0 (m ³ /s)
Displayed Precision	2

222
 223 In this study, both primary and secondary model parameters were utilized to enhance model accuracy. Primary
 224 parameters are the fundamental physical characteristics of the system, such as soil permeability, aquifer properties
 225 (like hydraulic conductivity), and elevation maps, which directly influence the model's behavior. Secondary
 226 parameters, derived from the primary data, were used to refine the model or simulate specific phenomena. For
 227 example, land use maps, rainfall data, and water quality data (such as EC data from wells) were used to improve the
 228 simulation of the aquifer's behavior, particularly in assessing human impacts and groundwater quality.

229 The results of the calibration and validation processes indicate that the model has successfully simulated
 230 groundwater level fluctuations with high accuracy (Figure 2a). The residual error analysis shown in Figure 2b
 231 confirms that the model's predictions are close to observed values, with minimal error. This demonstrates the
 232 model's ability to predict aquifer behavior reliably, even in the validation stage. In conclusion, calibrated and
 233 validated with primary and secondary parameters, the model has been proven to simulate groundwater behavior in
 234 the Marvdasht-Kharameh aquifer accurately. This model can be a reliable tool for analyzing and forecasting future
 235 aquifer conditions and supporting decision-making in water management strategies.

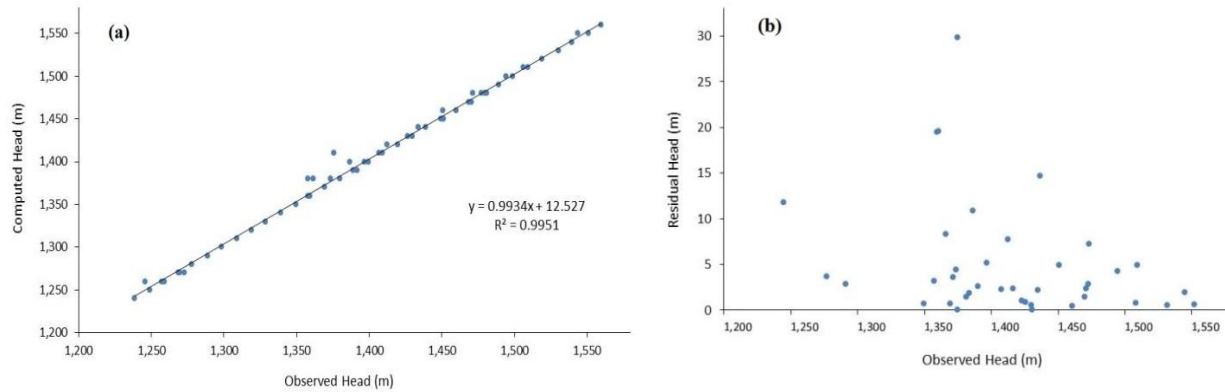


Figure 2. (a) A comparison between the predicted head and the observed value, and (b) Residual error of calculated values versus validation observation data

236
237

4. Results and Discussion

238 The mixing front in the Marvdasht-Kherameh aquifer exhibits dynamic behavior in response to varying conditions
 239 of groundwater extraction, recharge rates, and seasonal variations. Figure 3 presents the tolerance zones of the
 240 aquifer, categorizing regions into high-risk (red) and low-risk (blue) areas based on their susceptibility to saline
 241 intrusion and the movement of the mixing front. The red zones, representing areas of higher vulnerability, show
 242 rapid extension of the mixing front towards the freshwater zones during periods of increased groundwater
 243 extraction. This phenomenon is most evident in the southeastern regions, where higher extraction rates and reduced
 244 recharge exacerbate salinity intrusion, shifting the mixing front inland. In contrast, the blue zones, indicating stable
 245 conditions, show limited movement of the mixing front, as these areas are either less affected by saline intrusion or
 246 experience more consistent recharge, keeping the boundary of the mixing front relatively stable. Our model
 247 simulations confirm these observations, with significant shifts in the mixing front observed during dry periods and
 248 high extraction rates. These findings highlight the importance of managing groundwater extraction to prevent the
 249 rapid encroachment of saline water into freshwater zones.

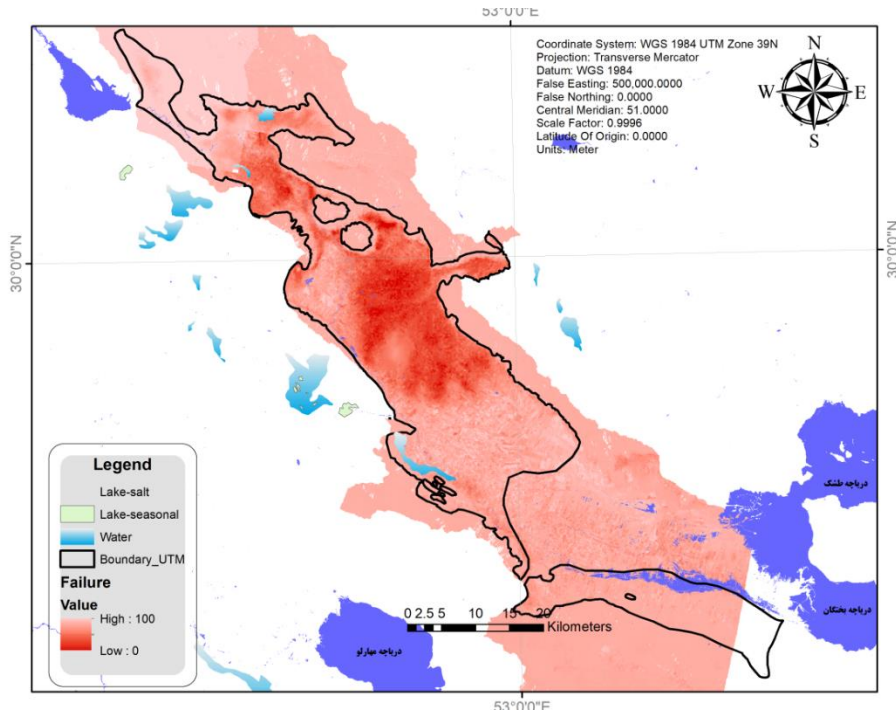


Figure 3. Tolerance zoning graph of saturated aquifer areas.

250

251 **4.1. Model Output Balance**

252 One of the most critical factors affecting the determination of the routing map, synonymous with the concept of the
 253 dispersion coefficient, is the flow budget. This concept, developed by the USGS (United States Geological Survey)
 254 for calculating the water balance in the MODFLOW model, is crucial. The results obtained from the Flow Budget
 255 applied in the calibrated MODFLOW model show that, on average, a specific share of the fixed aquifer storage
 256 decreases daily during the 127-month simulation period (Figure 4). This reduction, considering the decline in the
 257 groundwater level in the Marvdasht-Kherameh aquifer, is equivalent to a reservoir deficit of over ten years (Figure
 258 3a). Changes in the volume of in and outflow from the total boundaries (see Figure 1) with continuous loads are
 259 shown in Figure 4a, and the volume of recharge and discharge flows from the river networks are shown in Figure 4b

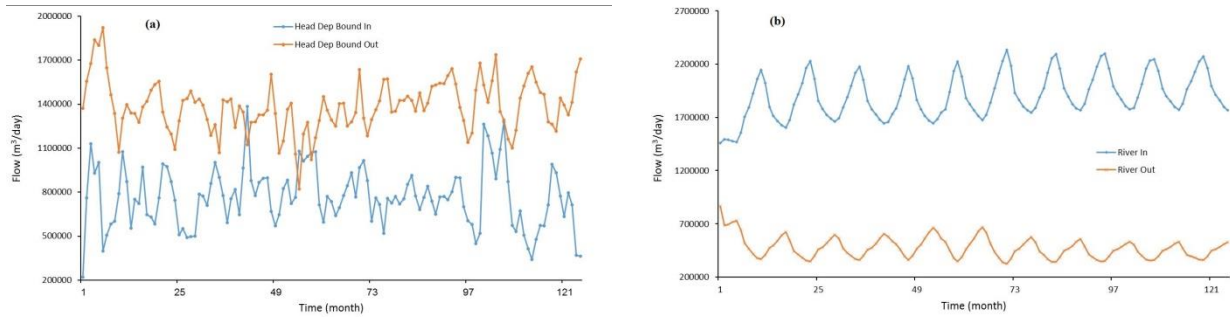


Figure 4. (a) The inflow and outflow from dynamic boundaries and (b) the volume of recharge and discharge from river networks in the Marvdasht-Kharameh plain.

260

261 In analyzing the Head Dep Bounds parameter shown in Figure 4a, it is necessary to state that this flux is defined at
 262 the boundaries of each border cell, with changes in the head of in and outflows to that cell, considering the relevant
 263 head and dependent drainage boundary, as specified in the software packages. This flux is expressed in the software
 264 output. Figure 4b shows the groundwater inflow (recharge) volume to the aquifer area under study, including
 265 groundwater inflow from the highlands. In Figure 4b, the outflow (discharge) volume from the study area's river
 266 network shows no permanent river (red path). Thus, the outflow volume from the plain is calculated using the
 267 MODFLOW. Considering the annual inflow volume from surrounding areas, it can be inferred that the inflow
 268 volume from the river network (blue path) in the Marvdasht-Kharameh aquifer has significantly decreased due to
 269 recent droughts.

270 Figure 5a shows the amount of water extracted by various exploitation sources (wells) within the study area's aquifer
 271 domain in different months. As can be seen from this figure, in the early months of the year, the amount of water
 272 exploited from the sources was much higher than in other months, and this trend has been almost stable for 8 years
 273 (2008 to 2016) or 127 months. Figure 5b illustrates the volume of in and outflow in the Marvdasht-Kharameh plain
 274 aquifer. As can be seen from the graph in Figure 5, with increased extraction from the aquifer in the study area,
 275 changes in the exchange volume of practical elements in the balance and a significant drop in the flow in the wells
 276 can be expected. Generally, according to Figure 5, it can be stated that the amount of water entering the area, in
 277 addition to being dependent on the physical conditions of the Marvdasht-Kharameh aquifer, such as hydrodynamic
 278 coefficients and gravity, directly depends on the pumping rate of the exploitation wells.

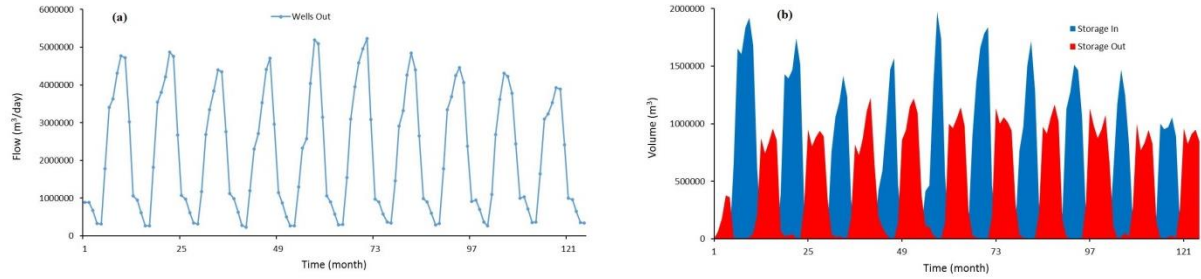


Figure 5. (a) Number of wells (flow out) and (b) The volume of water stored in the Marvdasht-Kharameh aquifer

279

280 **4.2. Model Output Water Level**

281 A model that has undergone calibration and validation is suitable for predicting the future state of the aquifer. It can
 282 determine future conditions under desired stresses to improve performance and make management decisions. Figure
 283 6 shows the groundwater level at the beginning of the 127-month analysis period for the study area aquifer and also
 284 shows the groundwater level at the end of the analysis period (127 months), considering the ongoing extraction
 285 (Figure 5a also shows this) from wells in the study area.

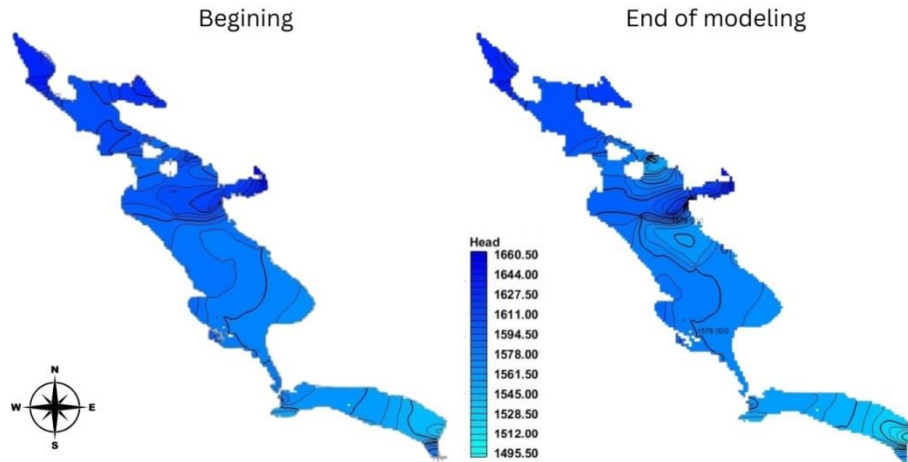


Figure 6. Groundwater level (m) of the Marvdasht-Kharameh aquifer for two periods, at the beginning and end (127 months), with continued extraction from wells.

286

287 In addition to the graphs shown in Figure 6, Table 3 summarizes the statistical status at the beginning and end of the
 288 127 months in the study area aquifer.

289

290

291

292

Table 3. Summary of statistical head status at the beginning and end of the 127-month study period

Period	Min Value (m)	Max Value (m)	Range (m)	Mean (m)	Median (m)	Standard Deviation (m)
Beginning of Analysis	1533.19	1660.27	127.08	1589.35	1585.58	22.36
End of 127-Month Period	1506.88	1660.27	153.39	1581.68	1578.74	24.61

293

294 Considering the raster finite difference charts in Figure 6 and the statistical summary in Table 3, excessive
295 groundwater extraction has decreased the water level in the Marvdasht-Kharameh aquifer over the approximately
296 11-year (127-month) study period.

297 Figure 7 represents a long-term prediction, extracted by applying restrictions and reducing extraction by 10% and
298 30% from the aquifer's exploitation sources, especially agricultural wells. These measures help stabilize the plain's
299 hydrograph and prevent further groundwater level decline.

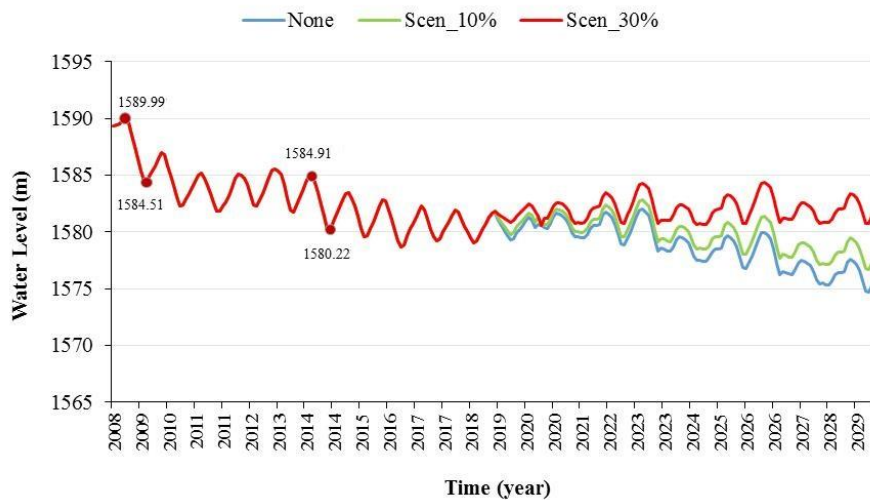


Figure 7. Unit hydrograph of the Marvdasht-Kharameh aquifer (finite difference network model output)

300 Based on the groundwater level map of the Marvdasht-Kharameh plain, the GMS software environment tools can be
301 used to draw groundwater flow velocity and direction lines for the entire aquifer area according to the magnitude
302 classification. The sudden drops at the four points are due to the 10% and 30% reduction in water extraction from
303 the aquifer, particularly from agricultural wells. This initial decrease in extraction causes a temporary drop in the
304 water level as the system adjusts to the new conditions. These drops represent the aquifer's response to the changes
305 in water usage, which stabilizes over time, leading to a more sustainable groundwater level in the long run. As
306 shown in Figure 8, the groundwater flow velocity in the middle parts of the aquifer is not too high. However,
307 significant changes in direction can be observed in these areas. The highest velocity vectors are visible in the

308 boundary areas and near the porous borders. Thus, it can be stated that the drilling of numerous high-extraction
309 wells in various parts of the aquifer has led to heterogeneous flow velocity structures within the Marvdasht-
310 Kharameh plain.

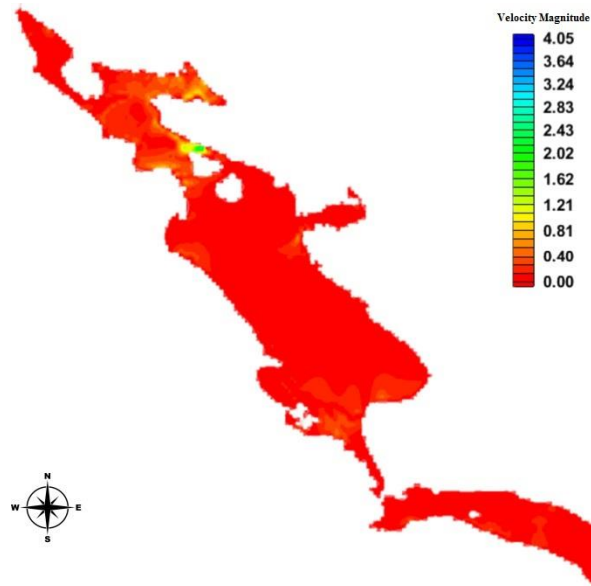


Figure 8. Velocity saturation of the final model of the Marvdasht-Kharameh aquifer

311
312 **4.3. Determination of the Dispersion Coefficient in the Tracking Model**

313 A drop in groundwater levels in an area can directly result in the infiltration of saline water from a wetland adjacent
314 to an aquifer. Predicting future conditions of the Marvdasht-Kharameh aquifer suggests that the current decrease in
315 groundwater levels may exacerbate these conditions. The MODFLOW model can forecast the unit hydrograph
316 changes over a period equivalent to the simulation period (127 months). As previously mentioned, the increase in
317 groundwater flow velocity in the aquifer can be influenced by artificial factors such as extraction sources or recharge
318 elements like basins and injection wells, as well as the residual structure of the aquifer. This means that increased
319 velocity in one area leads to a greater travel distance for particles (both saline and non-saline). The nature and
320 structure of the groundwater reservoir, independent of natural barriers, significantly impact the dispersion
321 coefficient.

322 Thus, the basis of uncertainty analysis calculations was derived from the dispersion coefficient analysis obtained
323 from groundwater flow simulations in the Marvdasht-Kharameh plain. The dispersion coefficient is a key parameter
324 for understanding the spreading of solutes, such as pollutants, within the groundwater flow system. The
325 MODFLOW groundwater flow model was used to simulate water movement through the aquifer. The MODPATH

326 model was then employed to track the movement of particles, providing insight into the paths of solutes and their
327 dispersion within the system. The dispersion coefficient was determined by analyzing these particles' travel
328 distances and distribution over time. To estimate the dispersion coefficient more accurately, Kriging interpolation
329 was applied to model the spatial distribution of particle movement across the aquifer, considering the heterogeneity
330 of the system. Kriging helped create a more detailed spatial map of the dispersion coefficient by accounting for
331 variations in particle movement at different locations within the aquifer. Additionally, First-Order Reliability
332 Method (FORM) was used to perform uncertainty analysis, which refined the spatial variability of the dispersion
333 coefficient and quantified the uncertainty associated with its estimation. This combined approach, utilizing
334 MODPATH, Kriging interpolation, and FORM, enabled a more accurate determination of the dispersion coefficient,
335 providing a deeper understanding of solute transport behavior in the aquifer and helping to assess potential
336 contamination risks.

337 After optimizing calibration parameters in the finite difference model output and utilizing the MODFLOW
338 mathematical model, water level elevations were generated for approximately eleven consecutive years following
339 the initial month of stable simulation in the GMS software. Based on the results of Figure 6, primary coefficients in
340 the MODPATH model were assigned to define the starting points for salinity analysis in all cells of the finite
341 difference groundwater flow network. With only one starting point, this method's results represent particle paths
342 across the plain.

343 In the next step, with the conversion of starting points to layering, spatial zonation was performed using the Kriging
344 interpolation method in GIS software after determining the particle travel distances for each coordinate. The layer
345 equation variogram setting and optimal parameter determination for the dispersion coefficient layer are shown in
346 Figures 9. Figure 9 illustrates the local parameters set by the Kriging interpolation method. In this figure, the vertical
347 axis represents semivariance (γ), a measure of the dissimilarity between pairs of data points as a function of the
348 distance between them. Semivariance increases as the distance between points grows, indicating that data points
349 farther apart become less similar or correlated. Essentially, it quantifies how much the data varies over space. The
350 greater the semivariance, the less correlated the two data points are. The horizontal axis represents the distance (h)
351 between pairs of data points in meters. It shows how the semivariance changes as the distance between the data
352 points increases. The relationship between semivariance and distance helps to quantify the range of spatial
353 correlation and is key for understanding the scale of spatial dependency in the dataset. The nugget refers to the value

354 of the semivariance at a distance of zero. This is the starting point of the curve and typically reflects measurement
355 error or the inherent variability at very short distances. In the plot, the nugget is represented by the initial rise of the
356 curve, often close to zero, which suggests minimal difference at very small distances.

357 The range is the distance at which the semivariance curve levels off and no longer increases significantly. Beyond
358 this distance, the data points lose spatial correlation, indicating the effective distance over which spatial correlation
359 exists. The sill represents the value where the semivariance curve flattens out. It is the upper limit of the
360 semivariance, reflecting the total variability in the data that can be explained by spatial correlation. After reaching
361 the range, the semivariance stabilizes at the sill, showing that spatial correlation is no longer significant.

362 The semivariogram models the spatial dependence between data points. Initially, as the distance between points
363 increases, the semivariance also increases, showing that the correlation weakens with distance. Once the distance
364 reaches the range, the semivariance stabilizes, indicating no further significant spatial correlation, which is
365 represented by the sill. The nugget reflects short-range variability or measurement error. This relationship is crucial
366 for understanding the spatial dependencies within the data and underpins geostatistical methods like kriging.

367 Additionally, the model shown in the semivariogram represents the fitted mathematical model that describes the
368 spatial structure of the data. This model is fitted to the experimental data points (red dots), with the curve (blue line)
369 representing the theoretical relationship between distance and semivariance. The binned points (red dots) represent
370 the average semivariance calculated for specific distance intervals, and the averaged points (blue crosses) provide a
371 smoothed version of the data for better visualization and model fitting.

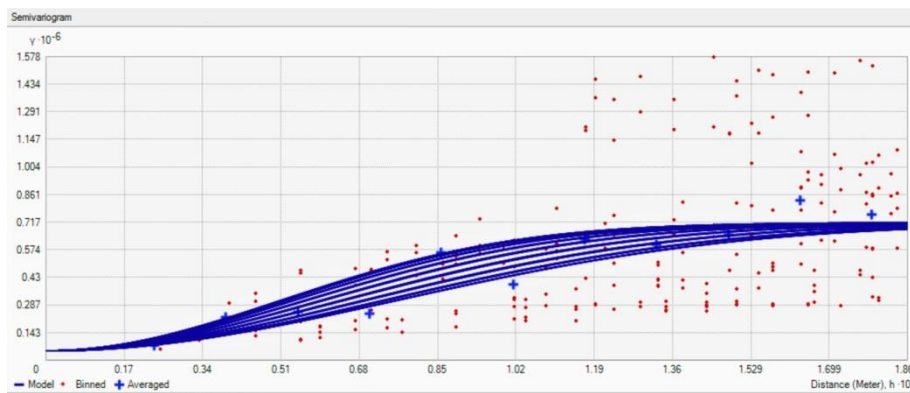


Figure 9. Parameters and variogram equation of zonation

372

373 According to Figure 9, when the distance between two points exceeds the range (1.869 m), the variogram's value
 374 approaches a constant value (0.71), indicating that the points are no longer spatially correlated. Also, a non-zero
 375 nugget effect indicates sudden changes at very small scales that larger-scale spatial models cannot explain. This
 376 indicates isotropy, meaning the spatial variability of dispersion is uniform in all directions. The error from the
 377 zonation process, if exceeding acceptable thresholds, will alter the extracted results heterogeneously.
 378 According to the FORM theory, the dispersion coefficient layer was extracted as raster layers in sequential intervals
 379 based on the homogeneous magnitude (Figure 9). Overall, the particle paths for the same starting points were
 380 extracted in four main categories: 1, 32, 64 months, and the end period (127 months). These layers were finally
 381 converted into a matrix network using their cell values. The dispersion coefficient matrix was placed in the FORM
 382 method performance equation (Eq. 4) to determine the reliability, measuring the change in particle dispersion speed
 383 from the end of the period to the beginning.
 384 To evaluate and analyze the spatial distribution of the transmissivity coefficient, a key parameter for groundwater
 385 exploitation, different geostatistical methods and distribution maps were compared using data from 240 deep wells
 386 (Figure 10).

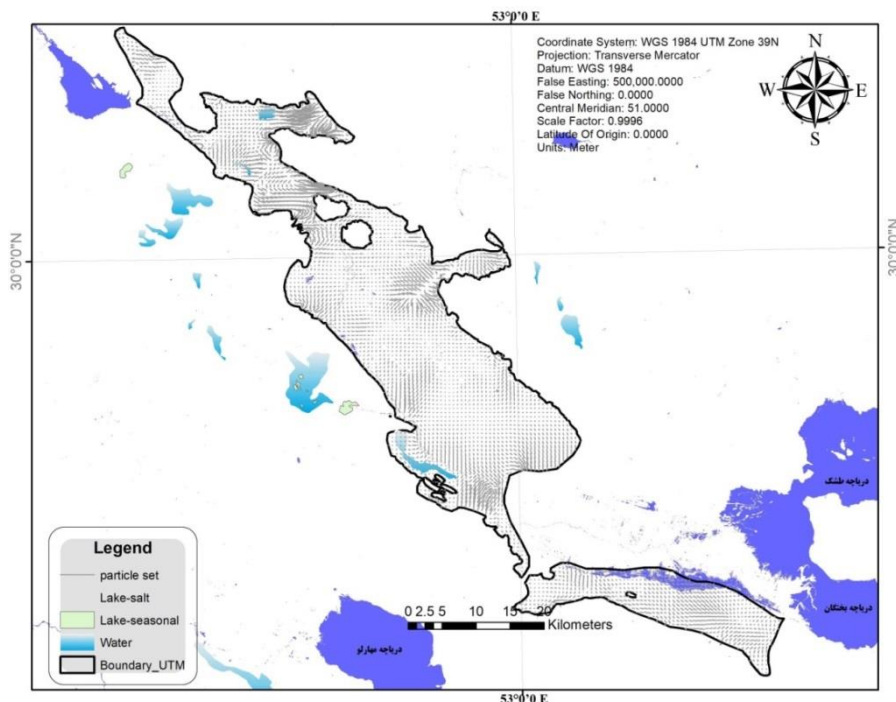


Figure 10. Transmissivity coefficient in the study plan at the end of the modeling period

387 For this purpose, the R^2 statistical parameter (Eq. 3) was used to evaluate these two methods. The results showed
 388 that the simple Kriging interpolation method with a correlation coefficient of 0.005 exhibits a good correlation. The

389 base value of the transmissivity coefficient, based on the path lengths obtained from the MODPATH model within
390 the Marvdasht-Kharameh aquifer at the end of the simulation period, is shown in Figure 11. The fundamental
391 assumption in preparing the function is to determine two periods of similar and independent lengths and to analyze
392 changes in dispersion velocity considering the destruction of porosity in the final simulation period. It should be
393 noted that the FP correlation coefficient is a statistical measure for evaluating the correlation between two nominal
394 variables in a 2x2 contingency matrix, with a value ranging between -1 and 1, indicating the strength and direction
395 of the relationship between two categorized variables.

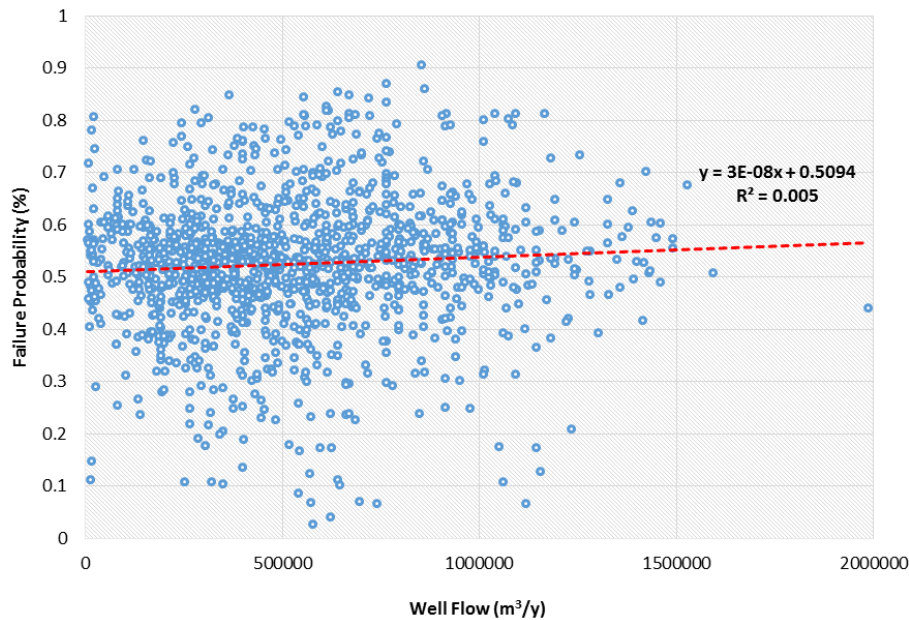


Figure 11. FP correlation coefficient and well discharge in the region

396 The very low correlation between the well discharge rates in the region and the failure coefficient at the exact
397 coordinates, as shown in Figure 11, indicates that the determination of restricted areas to prevent aquifer formation
398 destruction is not necessarily dependent on higher discharge rates.

399 The red dashed line in the plot represents a linear regression model that best fits the data. The slope of the line
400 (3×10^{-8}) indicates that the change in well flow has a minimal effect on the failure probability. The R^2 value of 0.005
401 suggests that the model explains very little of the variation in the data, meaning the relationship between well flow
402 and failure probability is not strong.

403 This study used reliability analysis methods, and probabilistic maps were extracted to identify the chances of
404 transitioning from stable flow dispersion conditions (flow velocity and direction, temperature, pressure, medium

405 density) to areas prone to disruption of the stable groundwater flow in porous media. Figure 12 shows the position of
 406 saline water bodies relative to the saturated aquifer boundary. Assuming seasonal variations in the groundwater level
 407 of the plain and the saline water bodies, this study questioned the probability of salinity intrusion into the aquifer.
 408 The FORM method and its specific outputs highlight areas where groundwater levels decrease. Suppose the aquifer
 409 structure and natural gravitational flow directions are suitable. In that case, water from the identified saline bodies
 410 and wetlands will infiltrate the groundwater reservoir to compensate for the storage deficit.

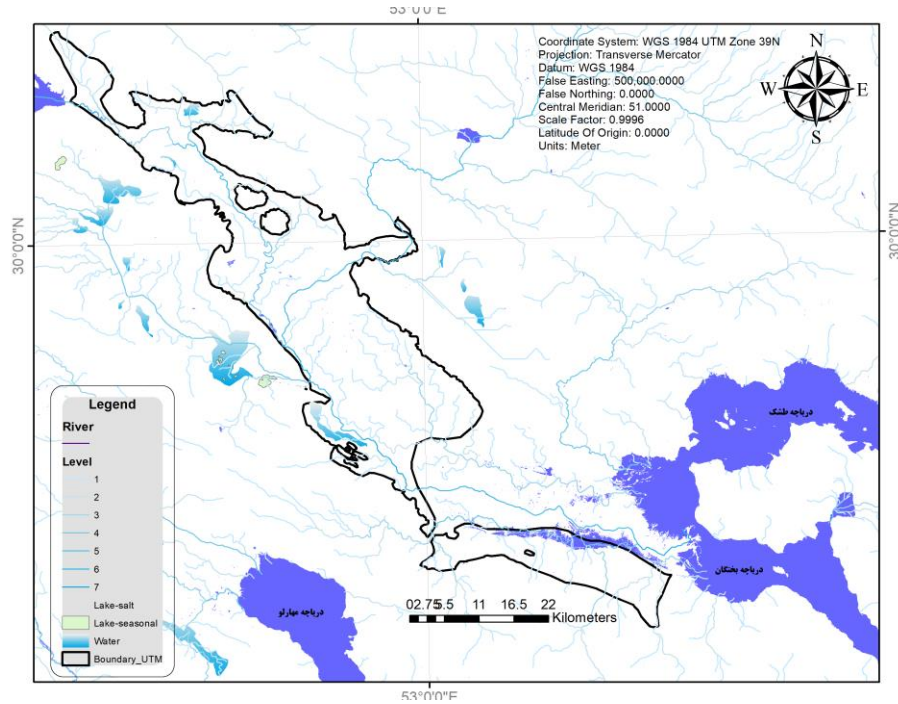


Figure 12. Position of saline water bodies relative to the saturated aquifer boundary.

411 The coefficients determined for all cells during the mentioned period were extracted using a linear regression
 412 equation in a spreadsheet environment, and the standard deviation was similarly calculated for 4035 cells. The
 413 importance function equation in the FORM method (Saghafian et al. 2021) is defined by Eq. (5):

$$G(x) = x_2 - x_1 \quad (5)$$

414
 415 In this equation, x_2 represents the average value of the dispersion coefficient in each cell in the 95th month, and x_1 is
 416 the same value in the 32nd month. In other words, by executing the reliability analysis method's computational code,
 417 written in Python using the PyRe module, the final output, based on coordinates, allows for the creation of a
 418 continuous raster map zoned between each probable failure rate, where the percentage indicates the possibility of a
 419 reduction in the dispersion coefficient over the ten-year modeling period. Figure 13 also shows the beta index (β) of

420 failure probability (pink color) in the raster cells. This coefficient is highly consistent with the failure probability
 421 value in the numerical model's output. With a suitable estimation, the zonation can be represented as a raster layer,
 422 indicating the dispersion coefficient in the aquifer during the study period. In this study, "failure" refers to the
 423 probability that the groundwater flow system will undergo structural changes or degradation under given conditions,
 424 such as excessive groundwater extraction or salinity intrusion.

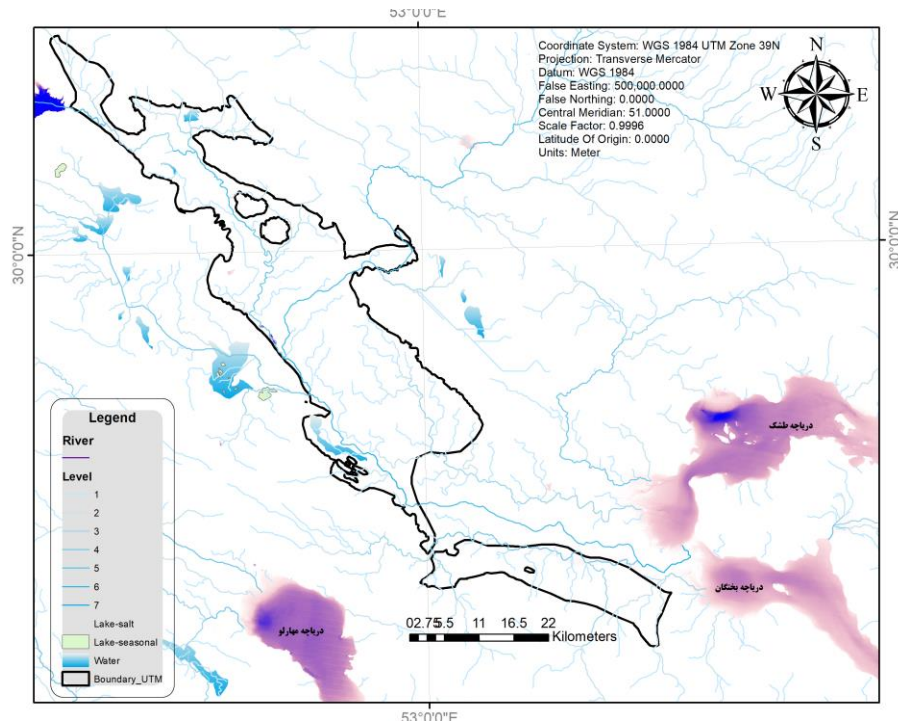


Figure 13. Occurrence percentage of saltwater bodies in front of a saturated aquifer

425 After preparing the matrix form of the diffusion coefficient layers in the inputs of the performance function equation
 426 and running the first-order reliability analysis method in the Python programming environment, the results are
 427 output as a matrix with maximum and minimum values of 6.98% and 0.011% for failure probability, respectively.
 428 As shown in Figure 3, determining restricted areas to prevent aquifer formation destruction is not necessarily
 429 dependent on higher discharge rates, and essential recharge parameters of the plain likely significantly impact flow
 430 displacement events. The failure probability in each case indicates the chance of flow path destruction in the raster
 431 cell of the study area. In Figure 3, the locations of areas with worse conditions in terms of tolerance against
 432 degradation and reduced water flow are shown in redder colors, according to the figure legend. The 50% probability
 433 indicates areas where structural changes will not cause significant damage to the flow network. Any value below
 434 50% inversely represents the chance of failure. Classes above 50% should be considered highly sensitive, restricted

435 areas. However, simple zoning based on parametric interaction is impossible for groundwater management. The
436 critical point is that the reduction zone for degradation, with decreasing density in the diffusion coefficient in areas
437 where the probability of failure is calculated to be less than 50%, is practically meaningless against the concept that
438 degradation in the flow layers is based on anthropogenic activities. In other words, although water accumulation in
439 the groundwater layers in some areas increases with the overall degradation of the aquifer network, this water is
440 extracted from the reservoir for local use, and with the continuation of current trends and considering pessimistic
441 climatic conditions, it leads to changes in the flow expansion pattern. Here, the probability of failure in each case
442 indicates the chance of structural failure in the raster layer cell of the study area.

443 According to the graph in Figure 14, it can be stated that in the Marvdasht-Kherameh aquifer, due to continuous
444 withdrawals by multiple exploitation wells during ten years from 2006 to 2016 (127 month), as well as the extension
445 of these conditions to the end of the hypothetical ten-year forecast period, and the potential for drilling illegal wells,
446 climatic changes, and drought occurrence leading to aquifer system depletion, changes in the diffusion coefficient in
447 the upcoming period will be very significant in some areas. The main reason for this is the high drop in groundwater
448 levels, which will be lost based on the destruction of the alluvial aquifer structure and the blockage of a large portion
449 of the voids that were considered the ultimate potential for water storage in the aquifer. The highest probability of
450 failure, meaning the most significant reduction in the aquifer's diffusion coefficient, will occur precisely in areas
451 previously identified as having high vulnerability based on three parameters: excessive drawdown, minimum
452 exploitation wells, and the highest dispersion coefficient in the final map.

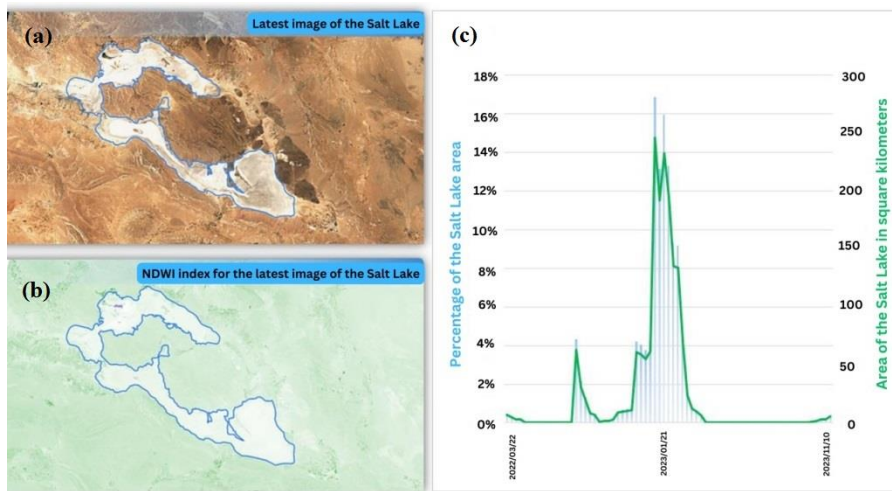


Figure 14. Time series of water availability in the wetlands of the investigated area in recent years. (a,b) latest image and NDWI index of salt lake and (c) percentage and area of the salt lake during time of study

453 One of the reasons for the unlikely infiltration of water into the aquifer is the lack of water sources within the
454 wetland area. Figure 14 shows that, based on satellite images, the chance of water presence in parts of the wetland is
455 less than 20%. Even in the best conditions, this value has not reached 100%. This situation has worsened in recent
456 years. The satellite images on the left side of Figure 14 illustrate the changes in the Salt Lake's water coverage. The
457 top photo shows the latest visible satellite image of the Salt Lake, outlining the current water boundaries. In contrast,
458 the bottom image displays the NDWI (Normalized Difference Water Index) for the same region, highlighting areas
459 with significant water coverage compared to dry land.

460 On the right side (Figure 14), the graph shows the time series data for two key metrics: the area of the Salt Lake in
461 square kilometers (green line) and the percentage of the Salt Lake's area (blue line). The sharp fluctuations,
462 especially in 2020 and 2021, with notable peaks, highlight the drastic changes in water availability in recent years.
463 These spikes indicate heavy rainfall or sudden water inflow, which has not been consistent over time.

464 The green line (Figure 14), representing the area of the lake in square kilometers, shows the physical changes in the
465 size of the lake, with notable increases during periods of significant rainfall, followed by sharp declines. The blue
466 line, showing the percentage of Salt Lake's area, emphasizes the relative changes in water coverage compared to the
467 total area. During peak water levels, the lake covered more than 16% of its location, but these levels have decreased
468 substantially during dry periods, reflecting the reduction in water availability.

469 This situation is critical because the aquifer's water level also drops as the lake's water level decreases. Therefore,
470 attention must not only focus on the aquifer's condition in terms of receiving water from surrounding areas but also
471 on the potential of these water sources within the wetland itself. The decreasing water levels, both in the lake and the
472 aquifer, point to a growing water scarcity problem, underlining the need for better water resource management to
473 address the challenges faced by this region.

474 Based on the results of this study, it can be concluded that the inability to implement comprehensive scenarios, such
475 as significantly reducing the extraction discharge of agricultural wells uniformly across the plain, highlights the
476 importance of the saline water intrusion from surface water sources. The failure probability ranges from a maximum
477 of 98% to a minimum of zero percent. The southern parts of the plain and the lower middle areas have a higher
478 chance of maintaining the permeability structure. However, these areas are also critical in the flow of salinity.
479 Considering that a decrease in the dispersion coefficient can be interpreted as a reduction in the aquifer's ability to
480 transfer flow, the forward trend suggests the recurrent intrusion of saline flow towards the aquifer and, consequently,

481 the drying of the wetland. The highest risk areas are in the plain's middle parts, indicating long-term salt
482 accumulation in the infiltration area.

483

484 **5. Conclusions**

485 This study provides a comprehensive and detailed examination of the dynamics of groundwater in the Marvdasht-
486 Kherameh aquifer, with a particular focus on the interactions between freshwater and saline groundwater. Through
487 the application of advanced modeling techniques, such as MODFLOW and MODPATH, the study simulates the
488 movement and behavior of the mixing front under varying conditions, including groundwater extraction, seasonal
489 recharge, and the impact of human activities. By modeling these factors, we have been able to better understand how
490 the mixing front responds to changes in aquifer dynamics and to identify the most critical factors that influence
491 salinity intrusion into freshwater zones. The results offer significant insights into aquifer management strategies,
492 particularly in regions vulnerable to salinity intrusion and over-extraction of groundwater resources. The key
493 findings of this study include:

- 494 • Models revealed that groundwater extraction plays a pivotal role in shifting the mixing front towards freshwater
495 zones, particularly in high-risk regions where extraction rates are higher. This indicates the need for careful
496 management to avoid salinity intrusion, which could compromise freshwater resources.
- 497 • The behavior of the mixing front was found to be significantly influenced by seasonal variations in extraction
498 and recharge. During dry periods, when extraction rates peak, the mixing front extends more rapidly,
499 particularly in high-risk zones. On the other hand, regions with higher recharge rates showed more stability,
500 with less movement of the mixing front.
- 501 • The sensitivity analysis demonstrated that hydraulic conductivity, salinity levels, and recharge rates strongly
502 affect the dynamics of the mixing front. Variations in these parameters caused significant shifts in the location
503 of the mixing front, highlighting their crucial role in the behavior of groundwater and salinity intrusion.
- 504 • The study emphasizes the importance of sustainable groundwater management in preventing salinity intrusion
505 and ensuring the preservation of freshwater resources. Effective strategies include optimizing extraction rates,
506 artificial recharge, and strategic well placement to maintain a healthy balance between fresh and saline
507 groundwater.

508 • Although the study provides robust insights into the mixing front's behavior, there is a need for further research
509 to incorporate real-time monitoring data into the models, allowing for more accurate and adaptive groundwater
510 management. Additionally, expanding the sensitivity analysis to include more detailed field data on hydraulic
511 parameters and salinity levels will improve the predictive accuracy of the models. Further exploration of
512 advanced modeling approaches that consider non-uniform flow and complex geological conditions will also
513 enhance our understanding of the aquifer's dynamics.

514 In conclusion, this research contributes significantly to the understanding of aquifer dynamics and offers practical
515 guidance for managing groundwater resources in arid regions. By combining advanced modeling, real-time data, and
516 sustainable extraction practices, future studies can improve water resource management strategies and contribute to
517 the long-term sustainability of aquifers in areas vulnerable to salinity intrusion and over-extraction.

518 While this study provides valuable insights, future research should focus on several key areas to enhance
519 groundwater management strategies. First, integrating real-time monitoring data into modeling can improve
520 predictions of the mixing front's movement, enabling more responsive and dynamic management of the aquifer.
521 Additionally, conducting a more detailed sensitivity analysis by incorporating parameters like hydraulic
522 conductivity, salinity levels, and recharge rates will refine the models and optimize management practices.

523 Future work should also explore advanced modeling techniques to account for non-uniform flow and aquifer
524 heterogeneity, improving predictions in complex geological conditions. Moreover, investigating sustainable
525 extraction practices, such as artificial recharge and well optimization, is essential to prevent salinity intrusion and
526 ensure the long-term health of the aquifer. Lastly, considering the impact of climate change on groundwater
527 dynamics will be crucial, as changing precipitation and temperature patterns could alter the behavior of the mixing
528 front.

529

530 **Declaration**

531 **Ethics approval and consent to participate**

532 Not applicable

533 **Consent for publication**

534 Not applicable

535 **Competing Interest**

536 The authors declare that they have no known competing financial interests or personal relationships that could have
537 appeared to influence the work reported in this paper.

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542 **Author contributions**

543 All authors contributed to the study's conception and design. Shahin Tavallali, Mahmoud F. Maghrebi, and
544 Mohammad Taghi Dastorani performed material preparation, data collection, and analysis. Shahin Tavallali wrote
545 the first draft of the manuscript, and all authors commented on previous versions. All authors read and approved the
546 final manuscript.

547 **Availability of data and material**

548 The data will be made available at a reasonable request.

549

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