- **Support Information**
- <sup>2</sup> Critical Threshold of 70 mol% CO<sub>2</sub> Concentration for
- **Economically Viable Geological Storage from Direct**
- 4 Air Capture (DAC)

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## Method

### **Temperature and Pressure Range**

This work selected 6 well-known CCS projects worldwide. The CarbFix project is a model for CO<sub>2</sub> mineralization research. Reportedly, the injected CO<sub>2</sub> reacts with basalt, achieving permanent disposal within just two years<sup>1,2</sup>. The Cranfield project, located in Mississippi, USA, features high temperature and pressure conditions.<sup>3</sup> Sleipner<sup>4–6</sup> and Decatur<sup>7,8</sup> are among the world's earliest CCS projects, whose designs and processes have served as references for many subsequent projects. Nagaoka is the first Japanese pilot project for CO<sub>2</sub> geological storage<sup>9,10</sup>. The China Offshore project is one of the country's latest CCS initiatives, with significant storage potential<sup>11</sup>.

Table S1 Typical CO<sub>2</sub> Storage Site Worldwide

Field Project and Location	Temperature (°C)	Pressure (Bar)
CarbFix, Iceland	20 - 33	~ 60
Cranfield, USA	120	324
Nagaoka, Japan	48	108
Sleipner, Norway	45	100
Decatur IBDP, USA	50	221
China Offshore, China	~90	254

#### **Force Fields**

The field force used for CO<sub>2</sub>, N<sub>2</sub>, and O<sub>2</sub> was from TraPPE-small (Transferable Potential for Phase Equilibria), which is built to calculate small but vital molecules by the University of Minnesota<sup>12,13</sup>. These force fields were used by various studies, showing pretty good agreement in density and vapor-liquid equilibria calculation<sup>14–16</sup>. All Molecules built in TraPPE-small force field have rigid structures (i.e., no bonded potential) and do not otherwise fit into another TraPPE family. Detailed non-bonded parameters and partial charge can be found in Table S2. The Lorentz–Berthelot combination rules were employed to calculate the interactions among molecules. The density calculation uses the isothermal–isobaric (NPT) ensemble to validate the selected force fields for impurities.

Table S2 The Non-bond Parameters for Molecules

Table 32 The Non bond Larameters for Profession											
Molecules	Atom	$\sigma(nm)$	$\varepsilon(KJ/mol)$	q(e)	Critical Temperature(K) TraPPE-model / NIST	Critical Pressure (Bar) TraPPE-model / NIST					
$CO_2$	C	0.2800	0.2244918	0.7000	306.2 / 304.21	77.7 / 73.843					
	0	0.2050	0.6560464	0.2500							
	O	0.3050	0.6568464	-0.3500							
$N_2$	N	0.3310	0.2993040	-0.4820	126.5 / 126.19	34.6 / 33.98					
1 12	11	0.5510	0.2773070	-0.7020							
	MW	0.0000	0.0000000	0.9640							
	1,1,				1.50 5 / 1.51 50	<b>5</b> 0 <b>6</b> 0 <b>1 51 1</b>					
$O_2$	O	0.3020	0.4073860	-0.113	153.5 / 154.58	50.63 / 51.1					
	3 4337	0.0000	0.000000	0.006							
	MW	0.0000	0.0000000	0.226							

#### **Simulation Details**

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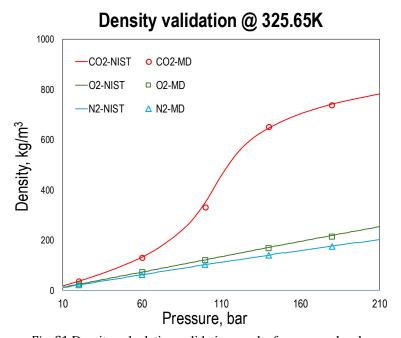
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All Molecule Dynamics (MD) simulations were performed with GROMACS package v2024.4<sup>17</sup>. The particle mesh Ewald (PME) method was applied for both long-range electrostatic and Lennard-Jones interactions with a Fourier spacing of 0.12 nm and a cutoff distance of 1.4 nm<sup>18,19</sup>. The bonds were constrained using a linear constraint solver (LINCS) algorithm with bond constraints added<sup>20</sup>. Additionally, 3-D periodic boundary conditions (PBC) were applied to all simulations. The ratio of N<sub>2</sub> to O<sub>2</sub> in the simulation is kept at 4:1. Each system contains 1,380 molecules. In all simulations, 3-D periodic boundary conditions (PBC) were applied to all simulations. The ratio of N<sub>2</sub> to O<sub>2</sub> in the simulation is kept at 4:1. Each system contains 1,380 molecules. For systems with different CO<sub>2</sub> concentrations, corresponding amounts of CO<sub>2</sub> were replaced with N<sub>2</sub> and O<sub>2</sub> in the same ratio. For example, under the condition of 50 mol%, the system contains 690 CO<sub>2</sub> molecules, 552 N<sub>2</sub> molecules, and 138 O<sub>2</sub> molecules. A total of seven typical cases are considered: 100% (pure CO<sub>2</sub>), 95mol%, 90mol%, 80mol%, 70mol%, 60mol%, and 50mol%. A  $10 \times 10 \times 10$  nm<sup>3</sup> box was prepared for holding molecules at the beginning stage. The system firstly relaxed through steepest descent algorithm (Energy minimization). After energy minimization, 1-ns NPT simulation with velocity-rescaling thermostat<sup>21</sup> and Berendsen barostat<sup>22</sup> was performed for equilibrium purpose. After that, 5-ns NPT simulation with Nosé-Hoover thermostat and an isotropic Parrinello-Rahman barostat was performed for production<sup>23–25</sup>. Time step was set as 1 fs, so there are 1,000,000 steps for equilibrium and 5,000,000 steps for production runs. Only the last 2 million steps of the final 5 million production simulation steps were used for result analysis, thereby avoiding any early-stage disequilibrium.

#### **Simulation Validation**

 The density of pure CO<sub>2</sub>, N<sub>2</sub>, and O<sub>2</sub> are calculated to validate the force field and computational method. Validation cases were conducted at a constant temperature of 325.65 K and varying pressures. The simulation results, presented in Fig. S1, show a strong agreement with NIST WebBook data<sup>26</sup>, with an average error of less than 1%. The results confirm the reliability of our simulation methodology and force field for accurate density predictions.



 $Fig. \ S1\ Density\ calculation\ validation\ results\ for\ pure\ molecules.$ 

# Radial Distribution Function (RDF) and Coordination Number

# 72 **Analysis**

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Besides the Lennard-Jones (LJ) potential and Coulomb potential investigation, we further analyzed the radial distribution functions (RDF) and coordination numbers (CN) for CO<sub>2</sub>-CO<sub>2</sub>, N<sub>2</sub>-N<sub>2</sub>, and CO<sub>2</sub>-N<sub>2</sub> pairs within the system. Fig. S1 a), d), and g) present the RDF distributions for CO<sub>2</sub>-CO<sub>2</sub>, N<sub>2</sub>-N<sub>2</sub>, and CO<sub>2</sub>-N<sub>2</sub>, respectively. The RDF peak values for different CO<sub>2</sub> concentrations were plotted against temperature, resulting in the curves shown in Fig. S1 b), e), and h). The CN values corresponding to the RDF valley following the first peak were also calculated and are presented in Fig. S1 c), f), and i). The peak data are influenced by concentration, leading to instability. For instance, Fig. S1 e) shows significant fluctuations in the RDF peak of N2-N2 under 90% CO2 conditions, while the CO<sub>2</sub>-CO<sub>2</sub> data remain stable. The CN trends displayed in Fig. S1 c), f), and i) reveal that CO<sub>2</sub>-CO<sub>2</sub> has a larger slope compared to N<sub>2</sub>-N<sub>2</sub> and CO<sub>2</sub>-N<sub>2</sub>, which show relatively minor changes in slope. A similar trend is observed in the first peak height plots, where the slope changes for N<sub>2</sub>-N<sub>2</sub> and CO<sub>2</sub>-N<sub>2</sub> are less pronounced. Notably, in the first peak height distribution of CO<sub>2</sub>-CO<sub>2</sub>, we observed a slope change similar to that in. The difference in values between the right and left sides of the plot is approximately 40.2%, consistent with the previously observed trends in density distribution and LJ potential.

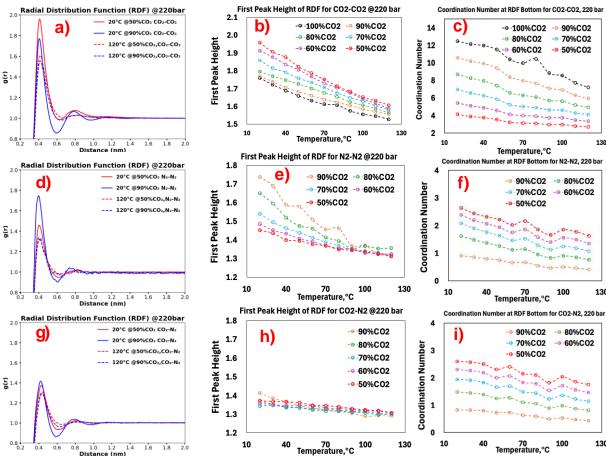


Fig. S1 Radial distribution function (RDF), RDF peak value, and coordination number for  $CO_2$ - $CO_2$ ,  $N_2$ - $N_2$ , and  $CO_2$ - $N_2$ .

## **Temperature and Pressure Gradient Profile**

A comprehensive investigation of pressure and temperature was conducted to establish the T-P relation, as shown in Table S3. Saline aquifers, conventional oil and gas reservoirs, shale, and coal beds are considered potential storage formations. In both sandstone and shale reservoirs, the common pressure gradient typically ranges between 90–120 bar/km, However, shale reservoirs in China exhibit higher pressure gradients, likely due to their greater burial depths. The temperature gradient range was not directly derived from the table data; instead, it was determined based on the global temperature distribution of sedimentary basins, making it a more representative selection. The formulas for pressure gradient and temperature gradient are as follows:

$$T - T_0 = K_T \times D \tag{1}$$

$$P = K_P \times D \tag{2}$$

where  $T_{\theta}$  is the initial temperature (°C),  $K_{T}$  is the temperature gradient (°C/km),  $K_{P}$  is the pressure gradient (bar/km), and D is the depth (km). P-T relation can be obtained by combining these two formulas.

106 Table S3 Comparison of the Temperature and Pressure Feature for CO<sub>2</sub> Storage Formation

Project and/or	Type of Reservoir	Water	Temperature	Pressure	Ref.
Location	Type of Reservoir	Depth, m	gradient, °C/km	gradient, bar/km	
Sleipner, Norway	The Utsira, Sandstone	90	33	100~110	4,5
Decatur, USA	Mt. Simon, Sandstone	Onshore	18.2	~103	27,7
Nagaoka, Japan	The Haizume, Sandstone	Onshore	33	98	9,10
Tomakomae, Japan	Volcaniclastic rocks and sand	20~40	~33	92~120	28
In Salah, Algeria	Carboniferous Sandstone	Onshore	~32	~100	29
Louisiana, USA	The Haynesville Shale	Onshore	25~33	103~109	30
South China	The Longmaxi Shale	Onshore	~33	150	31
N/A	A typical sedimentary basin	N/A	30	150	32
Texas, USA	The Barnet Shale	Onshore	~33	~100	33
N/A	A natural Coal Seam	N/A	25	150	34

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