

Skin-Integrated Electromechanical Systems for Characterization of Deep Tissue Biomechanics

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Supplementary Information

Supplementary Note 1

Supplementary Legends of Figures, Table and Movie

Supplementary Figure S1-S23

Supplementary Table S1

Supplementary Movie S1

Supplementary Note 1:

Finite Element Analysis (FEA). The commercial software ABAQUS was used to study the mechanical interaction among the actuator, Au sensor and tissues to be measured. The PDMS, phantom tissues and magnet were modeled by hexahedron elements (C3D8R) while the thin Au and Polyimide film were modeled by composite shell elements (S4R). The minimal element size was 1/5 of the width of the narrowest interconnects (50 μm). The mesh convergence of the simulation was ensured for all cases. The elastic modulus (E), Poisson's ratio (ν) and density (ρ) are $E_{\text{PDMS}}=1\text{MPa}$, $\nu_{\text{PDMS}}=0.5$, $\rho_{\text{PDMS}}=0.96\times 10^3\text{ kg/m}^3$, $E_{\text{Au}}=79\text{ GPa}$, $\nu_{\text{Au}}=0.4$, $\rho_{\text{Au}}=19.32\times 10^3\text{ kg/m}^3$, $E_{\text{magnet}}=113\text{ GPa}$, $\nu_{\text{magnet}}=0.34$, and $\rho_{\text{magnet}}=8.08\times 10^3\text{ kg/m}^3$, $E_{\text{PI}}=2.5\text{ GPa}$, $\nu_{\text{PI}}=0.34$, $\rho_{\text{PI}}=0.91\times 10^3\text{ kg/m}^3$, $E_{\text{Cu}}=119\text{ GPa}$, $\nu_{\text{Cu}}=0.32$, and $\rho_{\text{Cu}}=8.96\times 10^3\text{ kg/m}^3$.

References

1. Yu, X. et al. Skin-integrated wireless haptic interfaces for virtual and augmented reality. *Nature* **575**, 473-479 (2019).

Supplementary Figure Legends

Figure S1. Steps for fabricating and assembling EMM sensors. 1. Formation of electrical interconnects and strain gauges on glass wafers; 2. Transfer-printing procedure with a water soluble tape; 3. Printing onto a flexible layer of PDMS; 4. Assembly of the sensor with mechanical actuators, connected via wires and a PCB.

Figure S2. The strain sensor consisting of two-terminal Au wire connection embedded in polyimide layer, with (a) circuit diagram and (b, c) optical images of different locations.

Figure S3. Measurement setup for mechanical sensing that includes a current source, a lock-in amplifier and EMM sensor with external connection and biological measurement targets.

Figure S4. Robust mechanical properties of (a), (b) the flexible sheets of strain gauges and (c) the systems assembled with actuators, indicating that the sensors can be bent (a) and twisted (b) and the entire system can laminate onto a curved surface (c).

Figure S5. (a) Sensor resistance as a function of cycles of bending. Inset is an optical image of the sensor on a surface with a radius of curvature of 1.5 cm. (b) Bending tests and accelerated soak tests of the strain sensor. Inset shows an image of a sensor immersed in artificial sweat at 50 °C.

Figure S6. Systematic studies of the bending effects of EMM sensor measurements. (a) EMM sensors coupled on cylindrical substrates of PDMS with radius of curvature of 4 cm, 8 cm, 10 cm and ∞ cm, respectively. (b) Sensing voltages of EMM sensors with different bending radius.

Figure S7. Statistics on the resistance (strain sensor), yield, and the *SNR* (during measurements on cheek) of 100 fabricated devices. The yield corresponds to the percentage of functional devices.

Figure S8. Applications of EMM sensors on human subjects. The system can be placed in contact with various locations of human body such as the **(a)** forearm and **(b)** shoulder. An adhesive film (3M Tegaderm Film) laminated on top of the entire structure prevents motion during measurements.

Figure S9. Normalized amplitude-frequency response of the vibratory actuator in contact with an artificial skin sample with an modulus of 200 kPa.

Figure S10. **(a)** Schematic diagram of an EMM sensor coupled onto artificial skin samples (PDMS layers) on glass substrates, as an approximate mimic of the structure of device/skin/bones. **(b)** A collection of measurements of elastic modulus on different PDMS layers, as function of weight ratios of crosslinker, all tested by the commercial bio-indenter.

Figure S11. Recording of sensing voltages of V_S as function of actuation frequencies on artificial skin samples with elastic moduli of 200 kPa, without the magnets.

Figure S12. Simulated (line) and measured (symbols) V_S as a function of elastic modulus of the PDMS sample at 50 Hz, with constant thickness of 8 mm.

Figure S13. Results of experimental (E), FEA results and the fitting lines (Equation 1) of V_S as a function of sample thicknesses with various sample moduli.

Figure S14. Comparison of measurement results with EMM sensors on the same location of a human thigh with **(a)** hair bearing and **(b)** hairless regions. **(c)** The output sensing voltages show stable performance on both regions.

Figure S15. Schematic illustration of a simulated patient test. EMM sensors are coupled onto a silicone substrate (1 cm thick), with modulus of 500 kPa for the central part (1 cm diameter) and of 100 kPa for the surrounding part of the substrate that mimics the structure of a skin tumor, in an exploded **(a)** and cross-sectional **(b)** view.

Figure S16. Measurement results of the simulated patient test in *SI Appendix*, Figure S15.

Left: Photograph of the simulated patient test. Right: EMM sensor measurements of modulus values at the central and surrounding regions of the silicone substrate.

Figure S17. EMM measurements on (a) arm (b) hand and (c) lower back, with sensors on psoriasis lesion (right) and on nearby skin under normal conditions (left). Black frames correspond to the lesion regions of psoriasis.

Figure S18. Experimental results for sensing voltages from EMM sensors with (a) 3 mm diameter and (b) 1.5 mm diameter magnets as function of the thickness of artificial skin samples.

Figure S19. Simple estimation of tissue thickness in fingertip dorsum, with length measurements (a) from bottom of fingertip to nail plate; and (b) from bottom of fingertip to fingertip dorsum near the nail plate. The combined thickness for skin/tissues of fingertip dorsum near the nail root is ~ 3 mm.

Figure S20. FEA modeling to determine the modulus of skin and inner tissues for (a) cheek region and (b) fingertip dorsum from measurements using EMM sensors with different D . Here, E_A and E_B correspond to elastic modulus for skin and inner tissues. Insets show the photographs of the measurements.

Figure S21. Photograph of the strain sensor array on a polymer substrate during bent status.

Figure S22. (a) Photograph of the final, complete EMM mapping array laminated on an artificial skin (PDMS, 2 cm thick). Interconnections use flexible cable of heat seal connectors (HSCs). (b) The connection of the EMM array system to an external multiplexing board.

Figure S23. Schematic illustration of the DAQ system.

Table S1. The relationship between the elastic modulus E of tissues and $C(E)$ in Equation 1.

Movie S1. The video captured using a high-speed camera for vibration of magnet in slow motion at 50 Hz and V_A of 5 V.

Figure S1

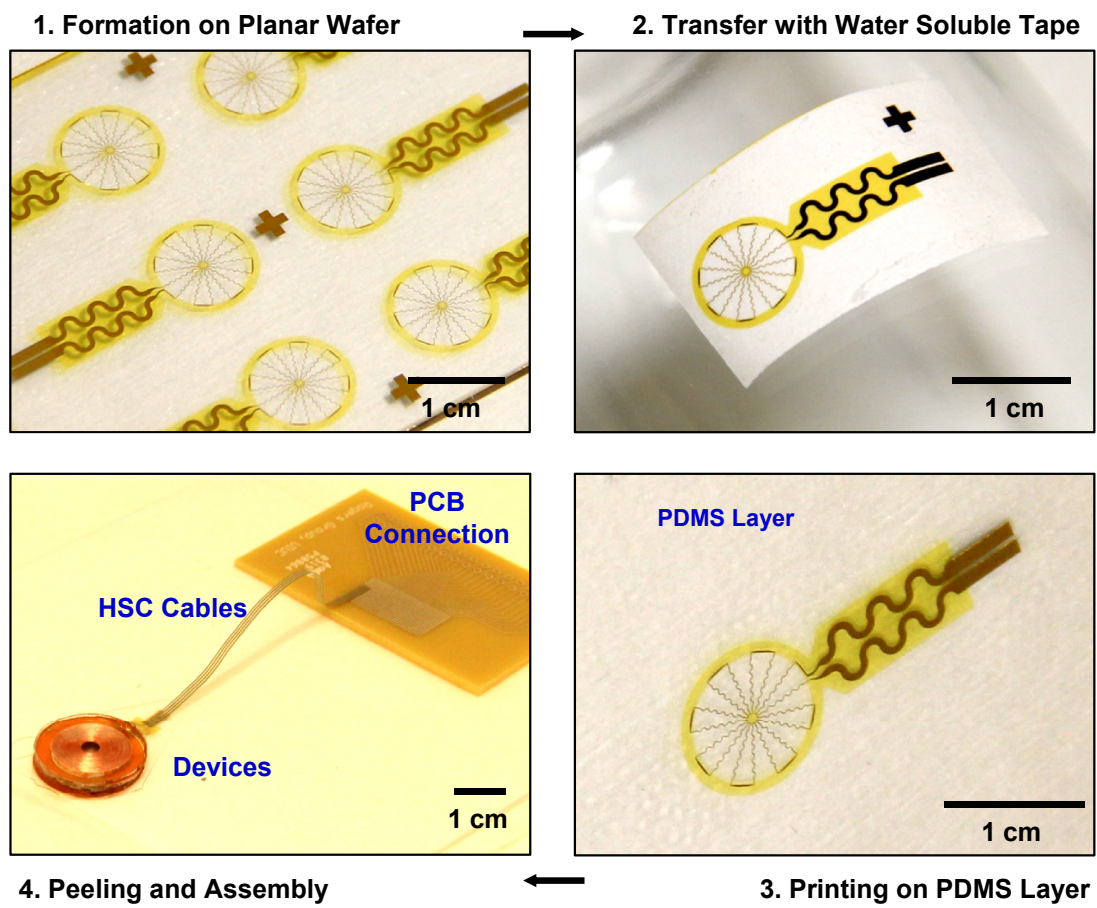


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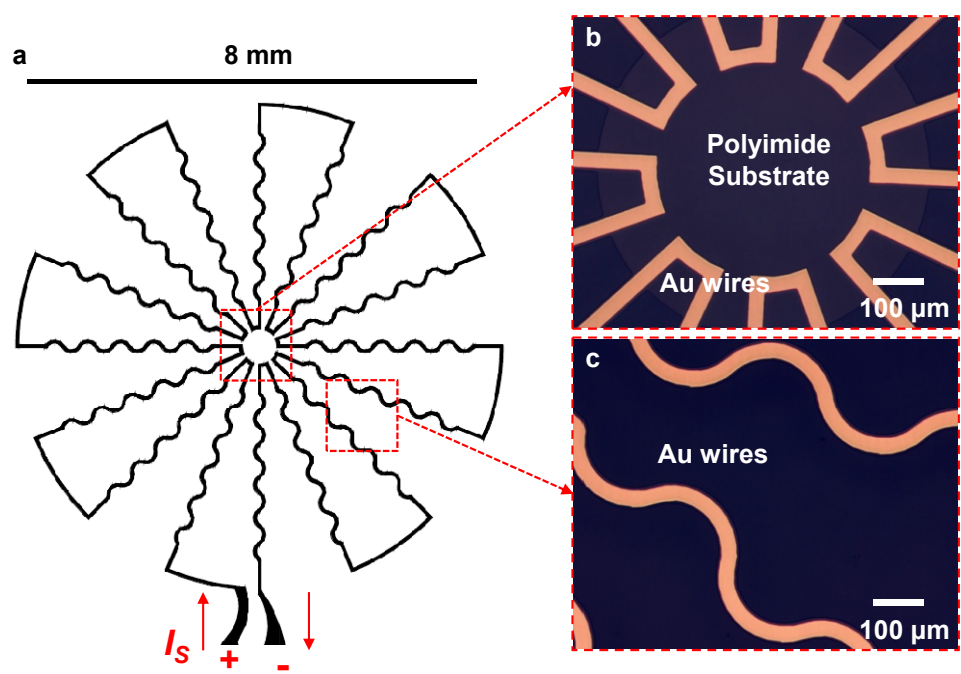


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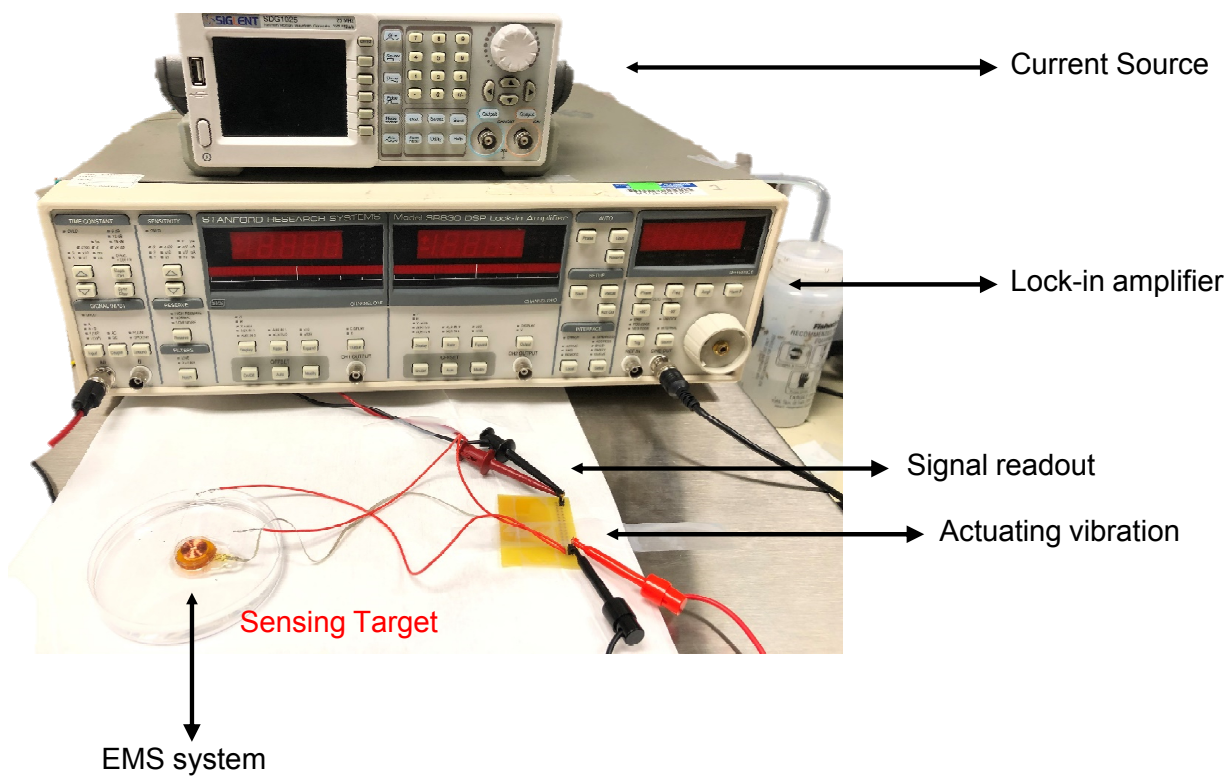


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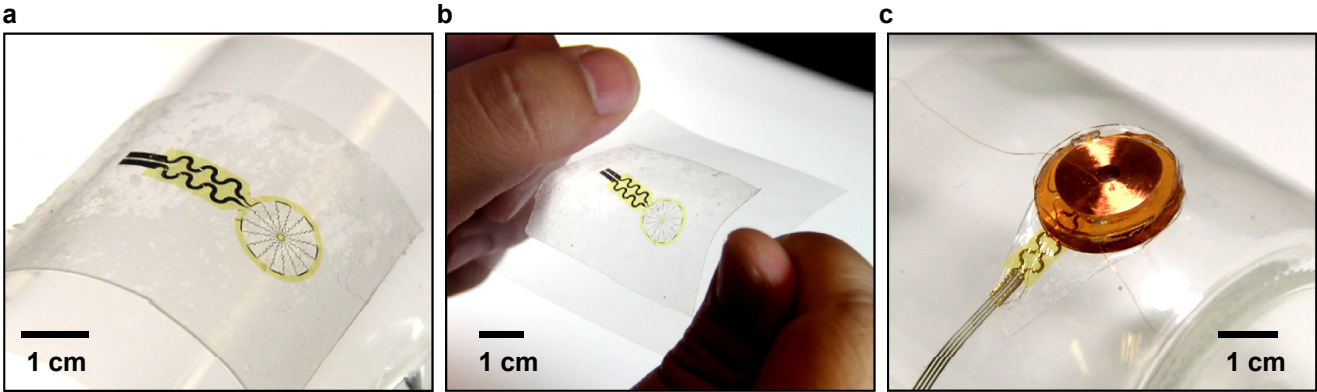


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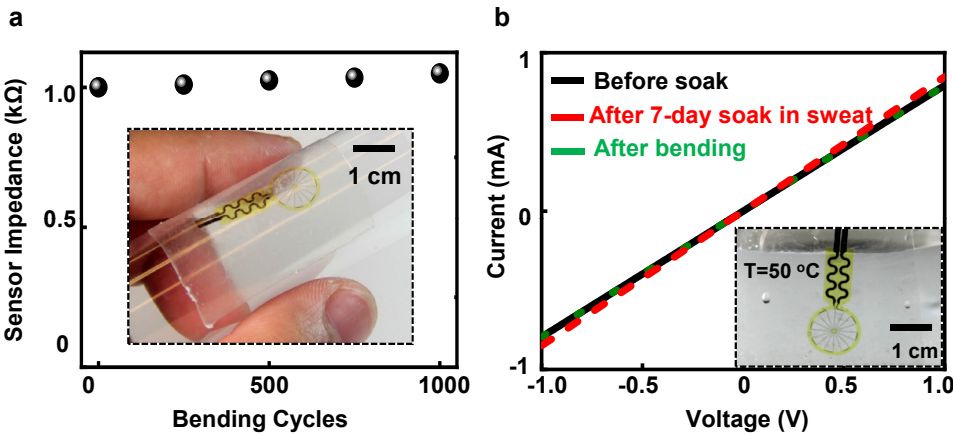


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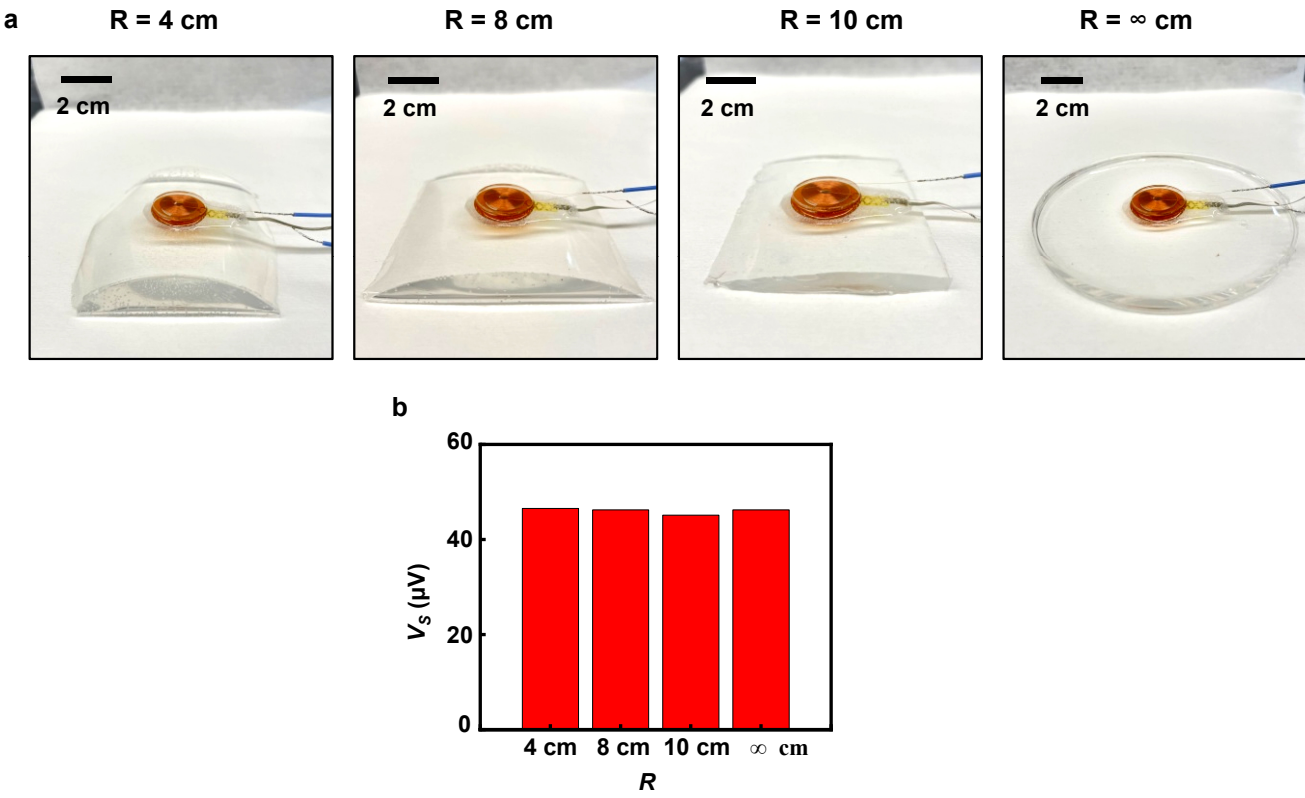


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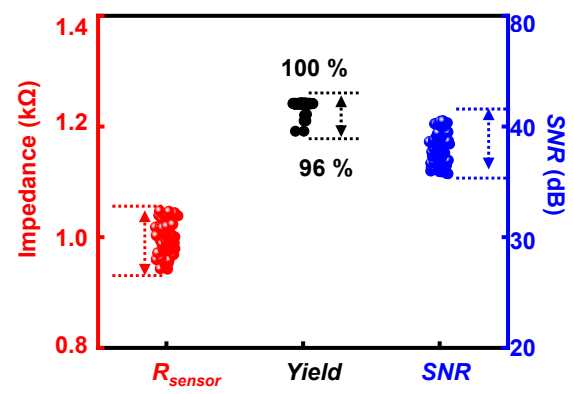


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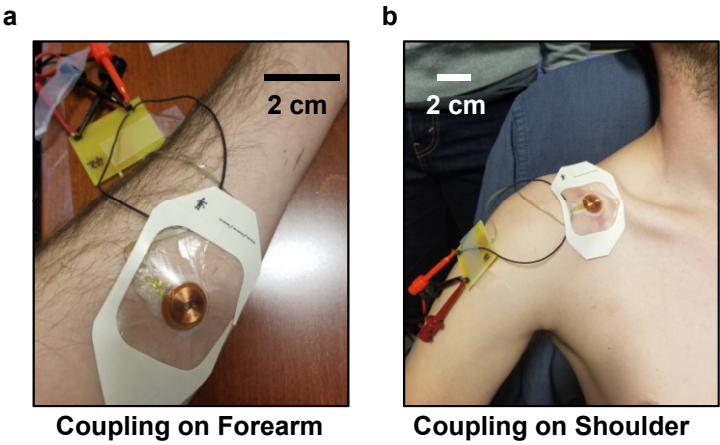


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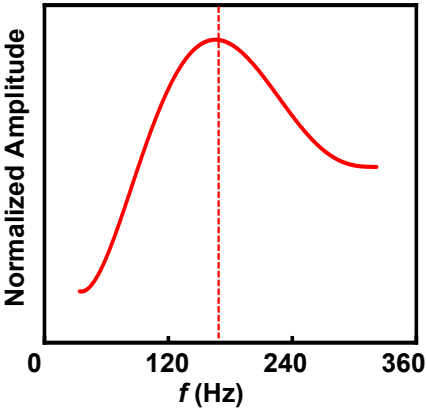
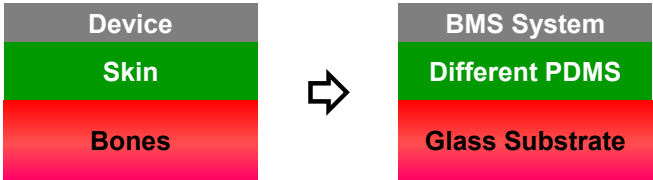


Figure S10

a



b

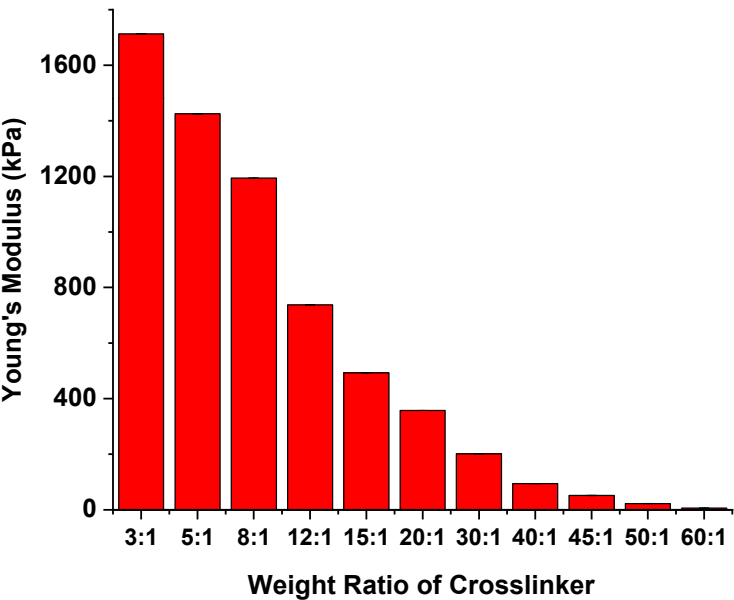


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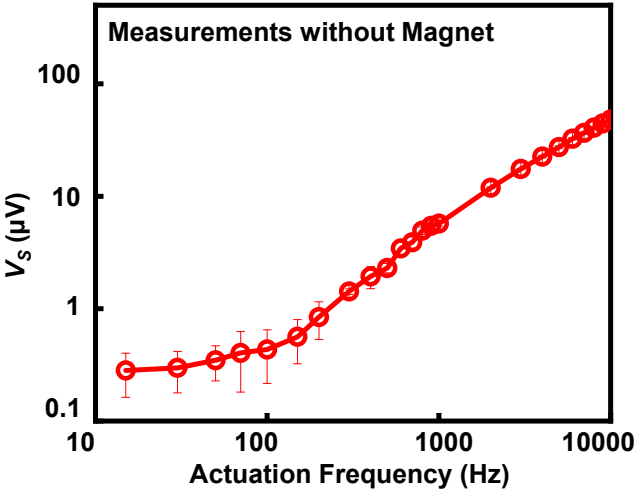


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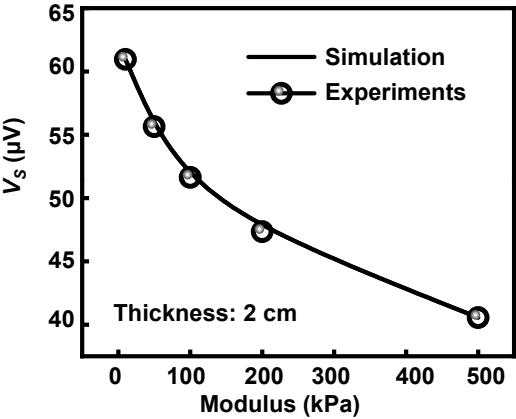


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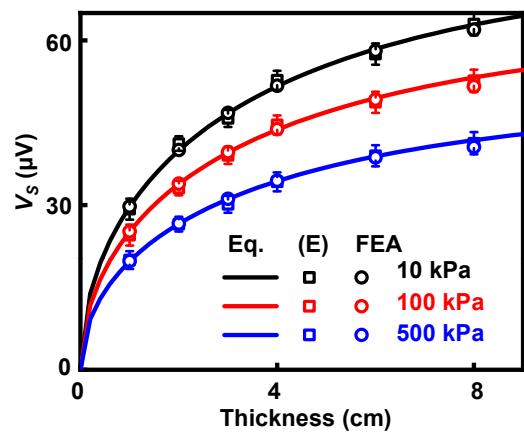


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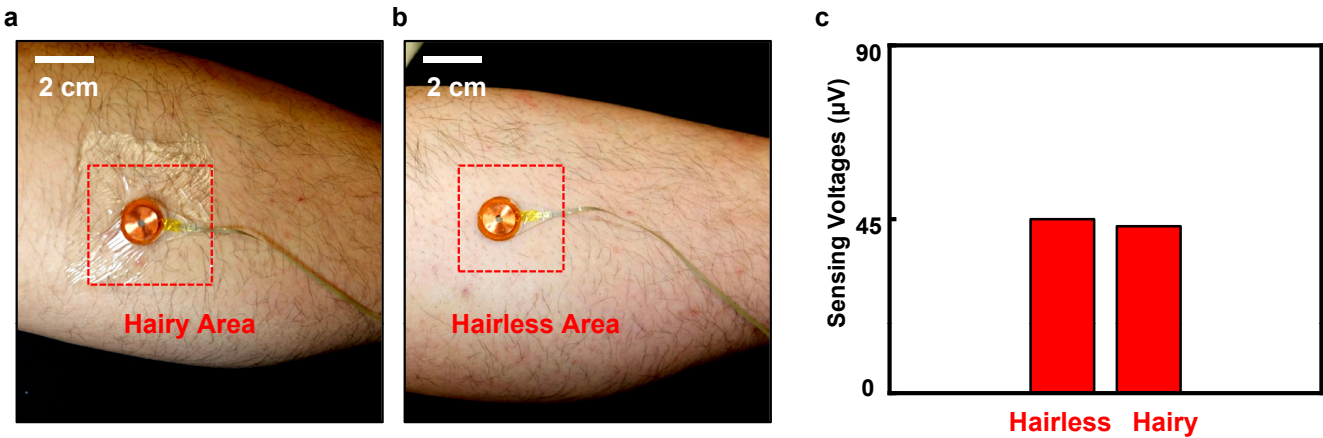


Figure S15

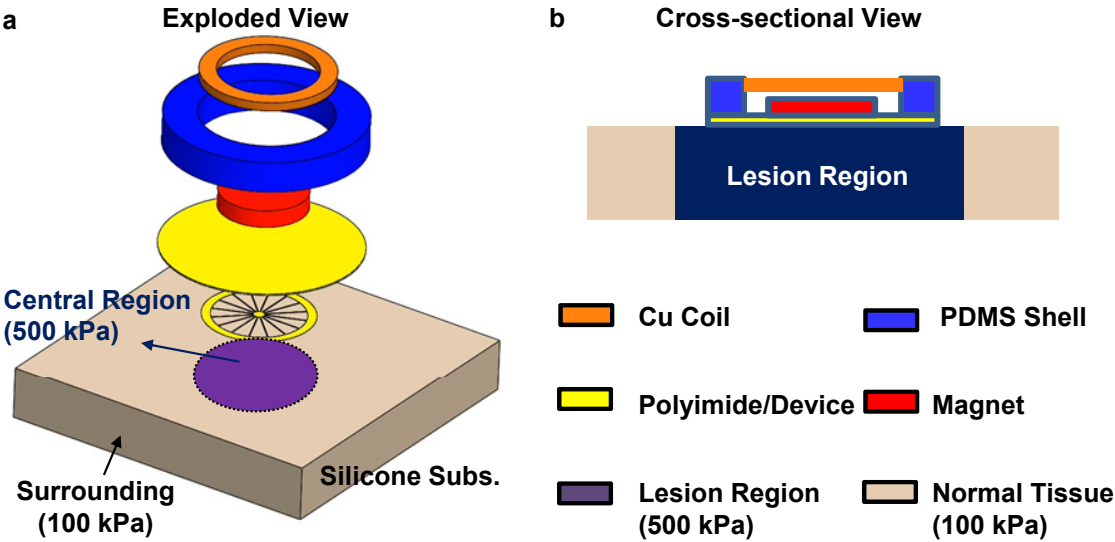


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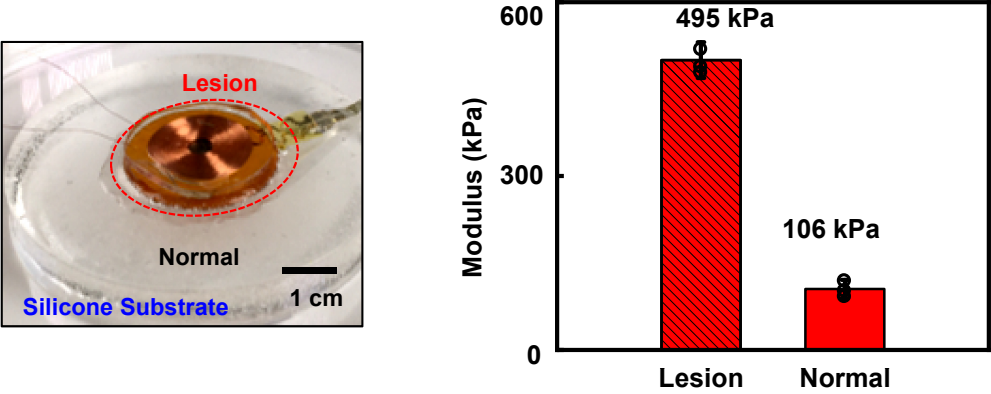


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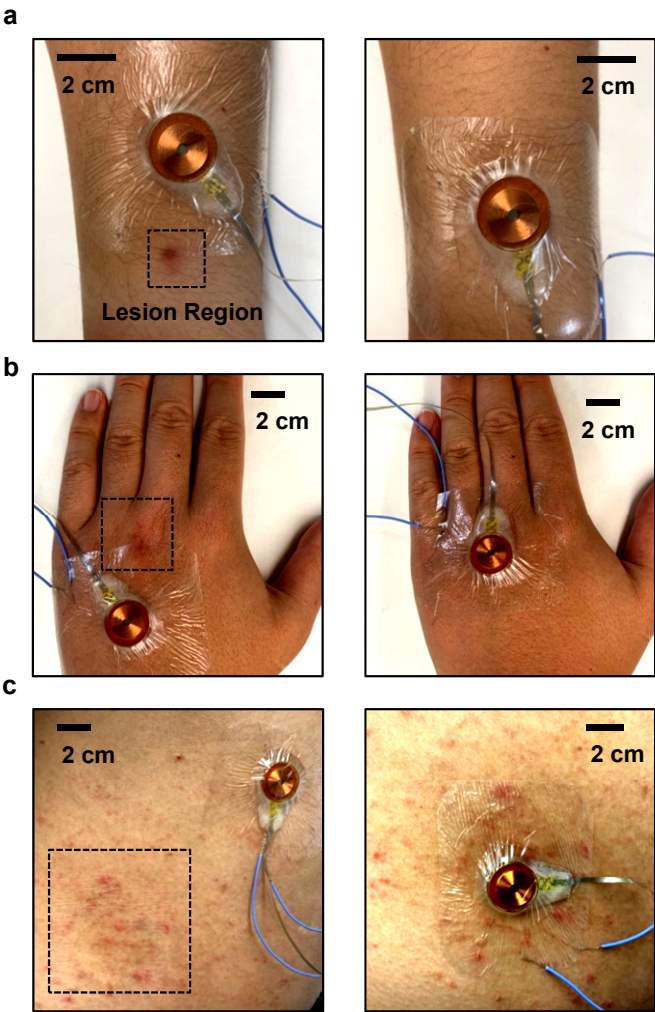


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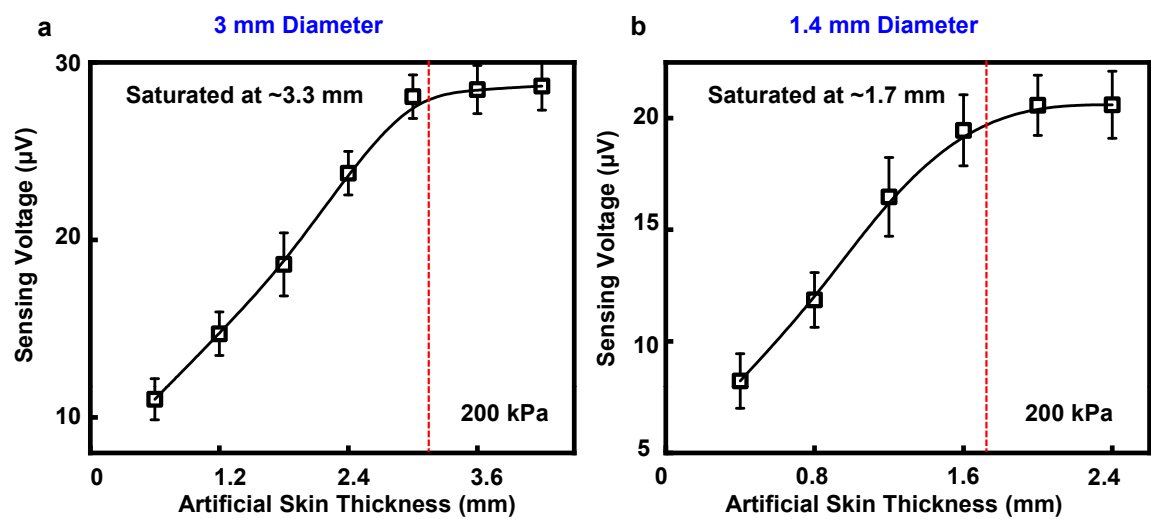


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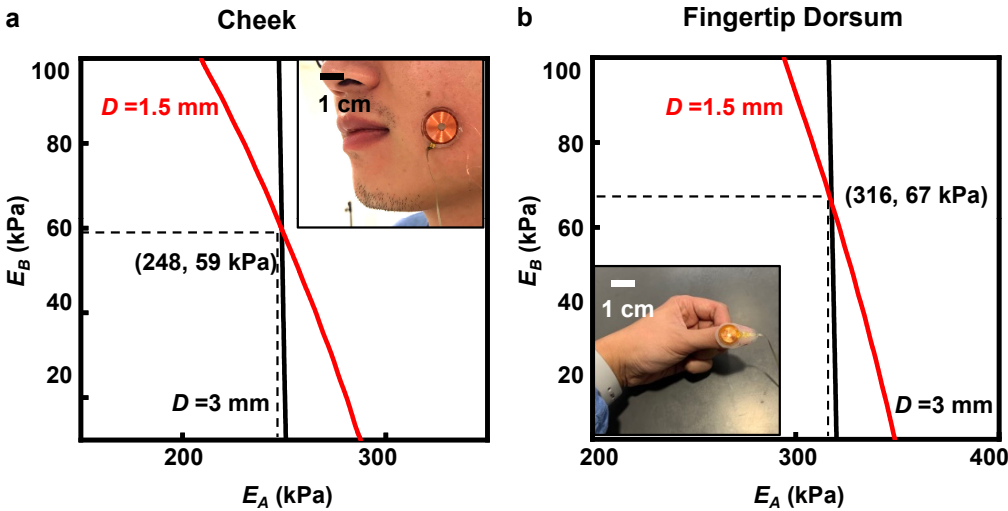


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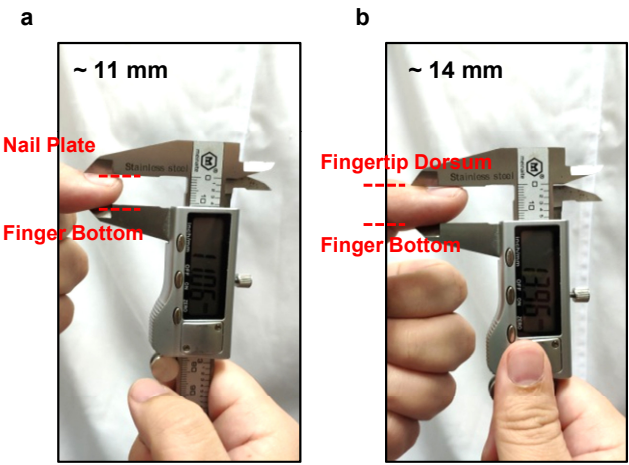


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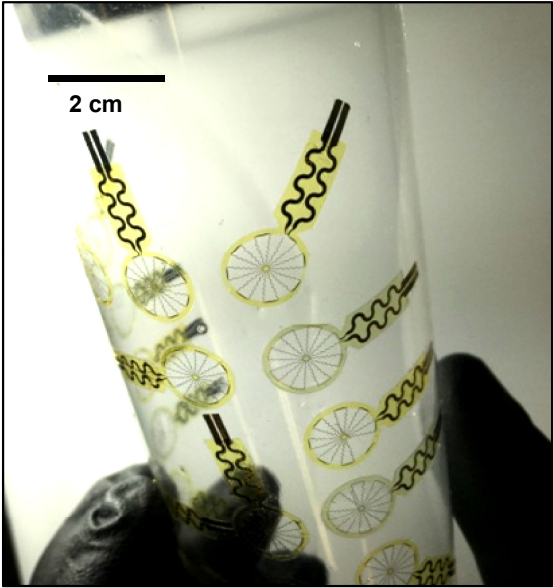


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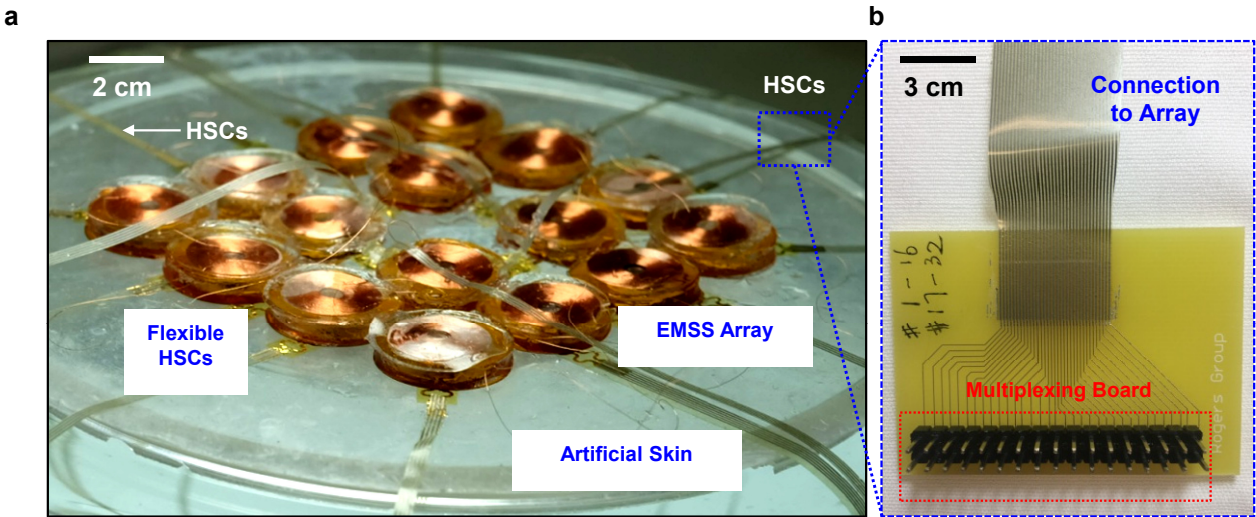


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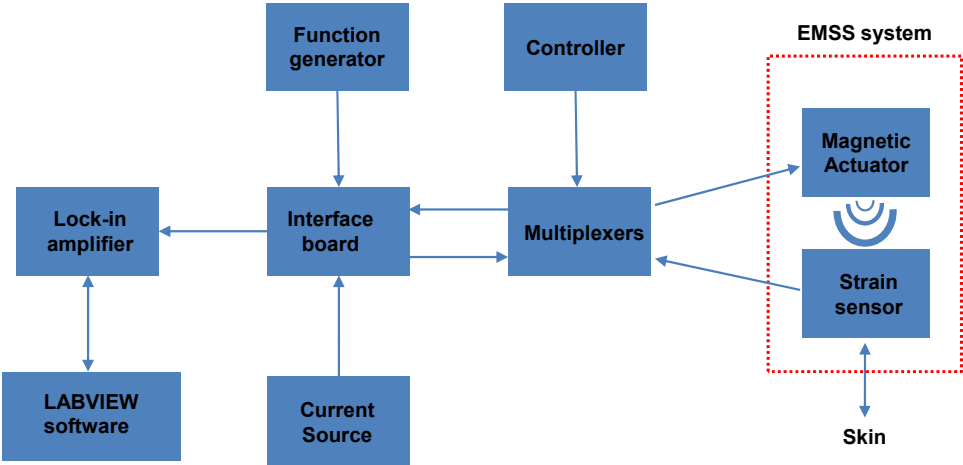


Table S1

E (kPa)	C(E)
10	1.53E-05
100	1.30E-05
500	1.02E-05

Table S1. The relationship between the elastic modulus E and C(E) in Equation 1.